



Semester Long Internship

On

**Development of Unit Operations and Binary Phase
Diagrams**

Submitted by

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Chapter 1

Introduction

Open Modelica is an open-source software which is based on the Modelica Language. It has various tools like OpenModelica Complier(OMC), Open Modelica Connection Editor (OMEedit), Open Modelica Shell(OMShell) and OpenModelica Python. Open Modelica is used for modelling, simulating, optimizing and analyzing steady state and dynamic systems. Open Modelica allows the users to write equations for a particular system and the solver solves the equations provided the number of equations is equal to the number of unknown variable. Open Modelica compiles the equations and functions into C code. The C code is combined with utility functions, run time library and a numerical Differential Algebraic Equation solver. OMEedit consists of several libraries for various domains like Electrical, Magnetic, Math, Thermal, etc. It provides various user friendly features like representation of a model in the form of block diagram. The Chemical process simulator(OMChemSim) which is being developed by FOSSEE Team at IIT Bombay provides an alternative to the various commercial software like ASPEN. OMChem has various unit operations and thermodynamic packages which makes it a very efficient tool for analysis.

Chapter 2

Distillation Column

2.1 Introduction

Distillation column is an unit operation which is used to physically separate a mixture into two or more fractions based on volatility of the components. The distillation column consist of trays for contacting vapour and liquid stream for effective mass transfer between the two phases. The vapour leaving from the top plate enters a condenser. The condenser can be a partial or total depending on the users preference. The condensate is collected in an accumulator and is separated into two streams L(Reflux) and D(Distillate). The amount of liquid reflux depends on the Reflux Ratio(RR) or L/D ratio. The liquid that leaves from the bottom tray enters the reboiler .In the reboiler the liquid is partially vapourised and the vapour is allowed to flow back into the distillation column and the liquid is withdrawn from the reboiler which is called as the bottom product(B).

The existing models for Distillation column provided in OMChem requires the user to write separate models to use condenser, reboiler, trays and distillation column. Each of the model is accompanied with thermodynamic package. In the existing model a rigorous procedure was employed using energy balances. This particular method made it difficult for the solver to solve the equation and would often result in convergence error. This is also made the model to be time consuming and less efficient. The primary objective of this work is to reduce the number of equations and improve the efficiency of the model.The distillation column that is build can be used for thermodynamic packages such as Raoult's Law and NRTL.

2.2 Modelling

The distillation column analysis is being done by Lewis Matheson Method. In this method to compute the composition and temperature of each stage in the distillation column it is necessary to obtain a solution to the following equations:

1. Equilibrium Relationships
2. Component Material Balances
3. Total Material Balances

The analysis of distillation column starts from the condenser and proceeds till the reboiler. The analysis is as follows:

At the Condenser:

The Lewis Matheson method by starts by assuming guess values for the distillate composition $x_{Di,guess}$ where $i=1,2,3,\dots,Nc$.

The vapour leaving from stage 1 has the same composition as the distillate $x_{Di,guess} = y_{1i}$ where $i=1,2,3,\dots,Nc$.

The liquid leaving from the condenser has the same composition as the distillate $x_{0i} = x_{Di,guess}$.

The vapour flow rate in mol/s leaving from the stage 1 is calculated by

$$V_1 = D + L_0$$

The reflux in mol/s that is entering the column is calculated by

$$L_0 = RR * D$$

The temperature at the condenser is determined using the bubble point equation :

$$\sum_1^{Nc} x_{Di,guess} * K_{Di} = 1$$

Where

K_{Di} depends on which thermodynamic package is chosen. In general it is given by

$$K_{Di} = \frac{y_{Di}}{x_{Di}} = \frac{\phi_{Di,L}}{\phi_{Di,V}}$$

Nc is the number of components.

D is the distillate flow rate in mol/s.

RR is the reflux ratio.

V_1 is the vapour flow rate in mol/s leaving from the stage 1.

L_0 is the reflux in mol/s entering the column.

$x_{Di,guess}$ is the guess composition value of distillate.

x_{0i} is the reflux composition.

y_{1i} is the composition of the stream leaving from stage 1.

Before proceeding with further analysis the vapour flow rates and liquid flow rates can be determined by using

Total Material Balance :

Across the entire column

$$\sum_{k=1}^{N_i} F_k = D + B + \sum_{k=1}^{N_{out}} S_k$$

Across each stage

$$f_j + V_{j+1} + L_{j-1} = V_j + L_j + s_j$$

j=1,2,3,...,Nt Where

F is the feed flow rate in mol/s

D is the distillate flow rate in mol/s

B is the bottoms flow rate in mol/s

S is the side flow rates in mol/s.

Nt is the number of stages in the distillation column

Ni is the number of feed Streams

Nout is the number of side streams.

f_j is the feed flow rate in mol/s that enters a particular stage.

V_{j+1} is the vapour flow rate in mol/s that enters a particular stage.

L_{j-1} is the liquid flow rate in mol/s that enters a particular stage.

V_j is the vapour flow rate in mol/s that leaves a particular stage.

L_j is the liquid flow rate in mol/s that leaves a particular stage.

s_j is the side flow rate in mol/s that leaves a particular stage.

In Lewis Matheson method the following assumption is valid that is equimolar flow of vapour

$$V_j + V_{fj} = V_{j+1}$$

where j =1,2,3,...,Nt-1

Where V_f is the vapour present in feed that enters the particular stage.

From the above the vapour flow rate from each stage is found out and the liquid flow rate from each stage is calculated by using total material balance for each stage.

The following procedure is used to calculate from stage 1 to reboiler

The temperature for a particular stage is being determined from dew point temperature formula.

$$\sum_{i=1}^{N_c} x_{ji} = 1$$

The equilibrium relation for each stage is given as follows:

$$y_{ji} = K_{ji} x_{ji}$$

Where

j=1,2,3,...,Nt and i=1,2,3,...,Nc.

y_{ji} is the vapour mole fraction of a particular component at a particular stage

x_{ji} is the liquid mole fraction of a particular component at a particular stage

K_{ji} depends on which thermodynamic package is chosen. In general it is given by

$$K_{ji} = \frac{y_{ji}}{x_{ji}} = \frac{\phi_{ji,L}}{\phi_{ji,V}}$$

The composition of the entering vapour stream can be found out using the component material balance of each stage.

$$f_j z_j + V_{j+1} y_{j+1,i} + L_{j-1} x_{j-1,i} = V_j y_{ji} + L_j x_{ji} + s_j w_{ji}$$

Where

j=1,2,3,...,Nt and i=1,2,3,...,Nc

z_j is the composition of the feed that is entering a particular stage

$y_{j+1,i}$ is the vapour composition that is entering a particular stage.

$x_{j-1,i}$ is the liquid composition that is entering a particular stage.

y_{ji} is the vapour composition that is leaving a particular stage.

x_{ji} is the liquid composition that is leaving a particular stage.

w_{ji} is the composition of the side stream that is leaving a particular stage.

Since an initial guess for the distillate composition is taken the condition to obtain the correct composition is given as follows:

The bottoms composition is calculated by using the guessed distillate composition with the help of overall component material balance

$$\sum_{k=1}^{Ni} F_k z_{ki} = D x_{Di} + B x_{obtBi} + \sum_{j=1}^{Nout} S_j w_{ji}$$

where i=(1,2,3,...,Nc-1)

The condition is imposed as follows where the difference between the calculated value from the analysis and the obtained value from the total component material balance should be 0.

The condenser and the reboiler duty is found as follows by energy balances:

Condenser duty is found by energy balance across the condenser

$$V_1 H_1 = L_1 h_1 + D H_D + Q_C$$

Reboiler duty is found by energy balance across the entire column

$$\sum_{k=1}^{Ni} F_k H_{fk} + Q_R = D H_D + B H_B + \sum_{j=1}^{Nout} S_j H_{sj}$$

Where

Q_C is the condenser duty in W.

Q_R is the condenser duty in W.

H_1 is the enthalpy of vapour in J/mol leaving the 1st stage.

h_1 is the enthalpy of liquid in J/mol leaving the condenser.

H_D is the enthalpy of the distillate in J/mol.

H_f is the enthalpy of the feed in J/mol.

H_B is the enthalpy of the bottoms in J/mol.

H_s is the enthalpy of the side stream in J/mol.

The enthalpy per mole of vapour and liquid leaving a particular stage can be expressed as

$$H_j = \sum_{i=1}^{Nc} H_{ji} y_{ji}$$

$$h_j = \sum_{i=1}^{Nc} h_{ji} x_{ji}$$

Where

j= 1,2,3,.....,Nt and i = 1,2,3,...,Nc

H is the enthalpy of vapour in J/mol.

h is the enthalpy of liquid in J/mol.

Since we have made an assumption of the vapour flow rate. The correct flow rates can be found by using the energy balances and the total material balance across each stage. The energy balance for each stage is given by

$$f_j H_{fj} + V_{j+1} H_{j+1} + L_{j-1} h_{j-1,i} = V_j H_{ji} + L_j h_{ji} + s_j H_{sj}$$

Where j=1,2,3,.....,Nt

H_f is the enthalpy of feed in J/mol.

H_{j+1} is the enthalpy of vapour entering a particular stage in J/mol.

h_{j-1} is the enthalpy of liquid entering a particular stage in J/mol.

H_j is the enthalpy of vapour leaving a particular stage in J/mol.

h_j is the enthalpy of liquid leaving a particular stage in J/mol.

h_{sj} is the enthalpy of side stream leaving a particular stage in J/mol.

2.3 Results

The following example was simulated and the results were compared with DWSIM.
System: Benzene and Toluene

The distillation column parameters and the feed conditions is given below

Condenser Pressure (Pa)	101325
Distillate(mol/s)	50
Feed stage location	3
Number of inlet	1
Number of side streams	0
Number of stages	6
Reflux Ratio RR	2
Reboiler Pressure (Pa)	101325
Guess Temperature Tguess(K)	360

Table 2.1: Distillation column parameters

Temperature(K)	298.15
Pressure(Pa)	101325
Flow Rate(mol/s)	100
Composition	
Benzene	0.5
Toluene	0.5

Table 2.2: Feed Conditions

The following results were obtained after simulation

Stages	x(-) Benzene	x(-) Toluene	y(-) Benzene	y(-) Toluene
Condenser	0.838931004	0.161068996	0.930988105	0.069011895
Stage 1	0.671505378	0.328494622	0.838931004	0.161068996
Stage 2	0.515678254	0.484321746	0.72731392	0.27268608
Stage 3	0.401205332	0.598794668	0.623429171	0.376570829
Stage 4	0.276230784	0.723769216	0.481250777	0.518749223
Reboiller	0.161068996	0.838931004	0.314618047	0.685381953

Table 2.3: Component Fractions in each stage

Stages	OM	DWSIM	Error percentage
	T(K)	T(K)	
Condenser	356.7318411	356.661	0.019862314
Stage 1	360.7146698	360.584	0.036238391
Stage 2	364.902247	364.713	0.051889304
Stage 3	368.3318454	368.067	0.07195576
Stage 4	372.4806425	372.494	0.003585974
Reboiler	376.7407085	376.866	0.033245639

Table 2.4: Temperature in each stage

Stages	Correct L(mol/s)	Correct V(mol/s)
Condenser	0	100
Stage 1	150	97.67614065
Stage 2	147.6761407	96.04156743
Stage 3	146.0415674	227.5145322
Stage 4	177.5145322	226.0838528
Reboiler	176.0838528	50

Table 2.5: Correct flow rates

The obtained condenser and reboiler duty is

	OM	DWSIM	Error Percentage
Condenser Duty Qc(W)	4748530	4744980	0.074815911
Reboiler Duty Qr(W)	-5865240	-5862210	0.051686992

Table 2.6: Condenser And Reboiler Duty

Chapter 3

Binary Phase Diagrams using Peng Robinson

3.1 Introduction

The Peng Robinson equation of state was developed by Ding-Yu-Peng and Donald Robinson in 1976. The Peng Robinson provides good accuracy near the critical point and for liquid molar volumes. It can be used to predict vapour liquid equilibria with good accuracy when combined with appropriate mixing rules.

3.2 Modelling

Peng Robinson (PR) Equation of state is given by

$$P = \frac{RT}{V - b} - \frac{a(T)}{V(V + b) + b(V - b)}$$
$$\alpha_i = [1 + \kappa_i * (1 - \sqrt{\frac{T}{T_c}})]^2$$
$$a_i = \frac{0.45724\alpha R^2 T_c^2}{P_c}$$
$$b_i = \frac{0.0778RT_c}{P_c}$$
$$\kappa_i = 0.37464 + 1.54226\omega - 0.26992\omega^2$$

For mixture consisting more than one component

$$a_{ij} = (1 - k_{ij}\sqrt{a_i a_j})$$

$$b = \sum_{i=1}^n x_i b_i$$

$$a = \sum_{i=1}^n \sum_{j=1}^n x_i x_j a_{ij}$$

Peng Robinson Equation of State based on compressibility factor:

$$Z^3 - (1 - B)Z^2 + (A - 3B^2 - 2B)Z - (AB - B^2 - B^3) = 0$$

$$A = \frac{aP}{R^2 T^2}$$

$$B = \frac{bP}{RT}$$

$$Z = \frac{PV}{RT}$$

The fugacity coefficient is calculated as follows:

$$\ln \phi_i = \frac{b_i(1 - Z)}{b} - \ln(Z - B) - \frac{A}{2B\sqrt{2}} \ln\left(\frac{Z + 2.414B}{Z - 0.414B}\right)\left(\frac{2 \sum_{j=1}^n x_j a_{ji}}{a} - \frac{b_i}{b}\right)$$

The equilibrium relations is given as follows

$$K_i = \frac{\phi_{i,L}}{\phi_{i,V}}$$

$$y_i = K_i x_i \quad (i = 1, 2, 3, \dots, Nc)$$

For Pxy:

Pxy is a binary phase diagram where the temperature is held constant. For a particular liquid phase mole fraction the pressure and vapour phase mole fraction is obtained by equilibrium equations.

Conditions for determining the pressure and vapour composition is

$$\sum_{i=1}^{Nc} y_i = 1$$

Initial pressure guess values is given by calculating the vapour pressure of the pure components at the specified temperature.

For Txy:

Txy is a binary phase diagram where the pressure is held constant. For a particular liquid phase mole fraction the temperature and vapour phase mole fraction is obtained by equilibrium equations.

Conditions for determining the temperature and vapour composition is

$$\sum_{i=1}^{Nc} y_i = 1$$

Initial temperature guess values is given by calculating the boiling point of the pure components at the specified pressure.

Nomenclature:

P is the Pressure (Pa)

V is the molar volume in m^3/mol

R is the gas constant $8.314 \text{ Pa.m}^3/\text{mol.K}$

T is the temperature (K)

P_c is the critical pressure for a particular component(Pa).

T_c is the critical pressure for a particular component(K).

ω_i is the acentric factor a particular component.

a is the Peng Robinson attraction parameter for the mixture.

a_i is the Peng Robinson attraction parameter for a paticular component.

b is the Peng Robinson co-volume for the mixture.

b_i is the Peng Robinson co-volume for a particular component.

k_{ij} is the Peng Robinson binary interaction parameter.

Z is the compressibility factor

ϕ_i is the fugacity coefficient for a particular component.

a_{ij} is the cross Peng Robinson attraction parameter for components i and j.

3.3 Results

Txy Results:

System: Ethane and Propane

Pressure(Pa): 101325

Number of Points : 6

The result obtained from the code is as follows:

x(-)(Ethane)	T(K) Temperature	y (-) Ethane
0	230.9289515	0
0.2	211.6561003	0.675565119
0.4	200.673366	0.867060687
0.6	193.5330955	0.942473334
0.8	188.3975618	0.979300095
1	184.4292755	1

Table 3.1: Txy Result for Ethane,Propane System

Pxy Results:

System: Propane and N-Butane

Temperature(K): 323

Number of Points : 6

The result obtained from the code is as follows:

x(-)(Propane)	P(Pa) Pressure	y (-) Propane
0	494268.6284	0
0.2	714942.7833	0.411429053
0.4	943508.0564	0.641867256
0.6	1182673.26	0.794098292
0.8	1436924.421	0.907112012
1	1714147.699	1

Table 3.2: Pxy Result for Propane, N-Butane System

The Txy and Pxy diagram for this particular system is given below in Fig 3.1 and 3.2 respectively.

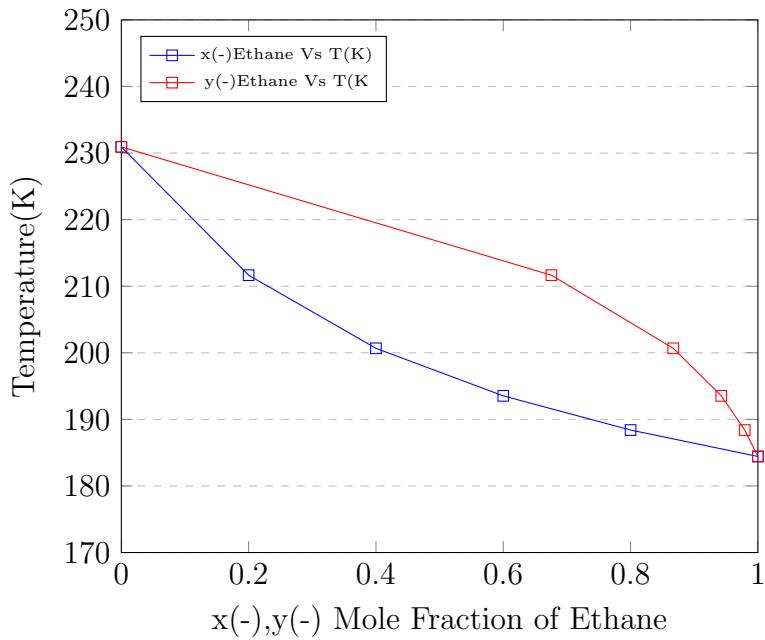


Figure 3.1: Txy Diagram of Ethane Propane System

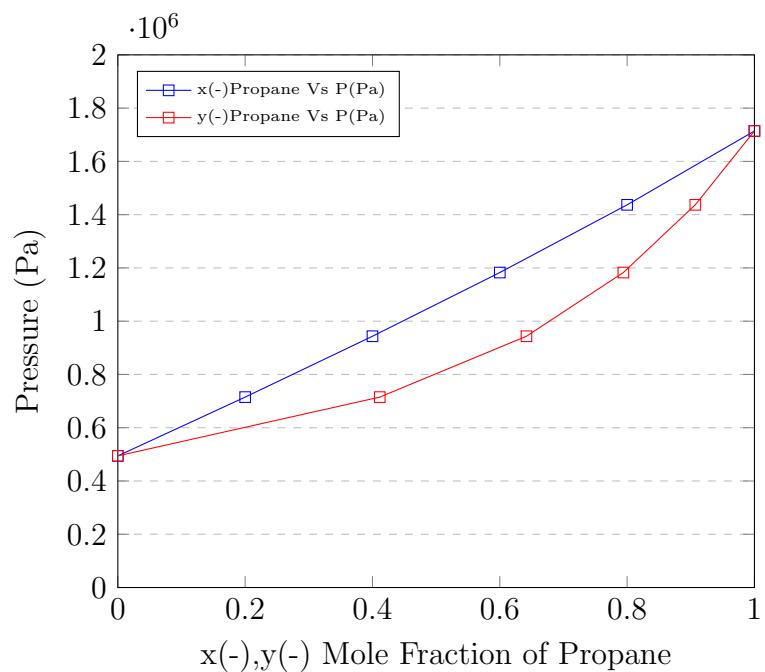


Figure 3.2: Pxy Diagram of Propane N-Butane System

Chapter 4

Equilibrium constant from Gibbs Energy of reaction

4.1 Introduction

The equilibrium reactor is a reactor for which equilibrium reactions can be specified. There are various modes to calculate and specify the equilibrium constant based on which the conversion is being calculated. The various modes are Gibbs energy of reaction, specifying the value directly or by specifying the coefficients of the equation if the equilibrium constant is expressed in terms of function of temperature. The primary objective of this work is to perform the calculation of equilibrium constant from the Gibbs energy of reaction.

4.2 Modelling

The equilibrium constant can be calculated as follows:

The standard state of enthalpy entropy and Gibbs free energy at 298 K is calculated as follows

$$\Delta H_R^0 = \sum_{i=1}^n \vartheta_i * \Delta H_{Fi}^0$$

$$\Delta S_R^0 = \sum_{i=1}^n \vartheta_i * \Delta S_{Fi}^0$$

$$\Delta G_R^0 = \sum_{i=1}^n \vartheta_i * \Delta G_{Fi}^0$$

Where

ϑ_i is the reaction stoichiometry

ΔH_{Fi}^0 is the enthalpy of formation

ΔS_{Fi}^0 is the entropy of formation

ΔG_{Fi}^0 is the Gibbs energy of formation

n is the number of components.

Enthalpy, Entropy and Gibbs Free Energy at Reaction Conditions:

$$\Delta G_R = \Delta H_R - T * \Delta S_R$$

Where

$$\begin{aligned}\Delta H_R(T) &= \Delta H_R^0 + \int_{T_{ref}}^T \Delta Cp dT \\ \Delta S_R(T) &= \Delta S_R^0 + \int_{T_{ref}}^T \frac{\Delta Cp}{T} dT\end{aligned}$$

For the given relations the specific capacity in J/mol.K is given by

$$Cp_i = aT^3 + bT^2 + cT + d$$

The ΔCp is given by

$$\Delta Cp = \Delta a * T^3 + \Delta b * T^2 + \Delta c * T + \Delta d$$

where

$$\Delta a = \sum_{i=1}^n \vartheta_i a_i$$

$$\Delta b = \sum_{i=1}^n \vartheta_i b_i$$

$$\Delta c = \sum_{i=1}^n \vartheta_i c_i$$

$$\Delta d = \sum_{i=1}^n \vartheta_i d_i$$

The constants a,b,c,d are predefined for each of the component. The constants are obtained by regression of the data of liquid and vapour specific heat capacity from DWSIM by using python.

$$\int_{T_{ref}}^T \Delta C_p dT = \frac{\Delta a(T^4 - T_{ref}^4)}{4} + \frac{\Delta b(T^3 - T_{ref}^3)}{3} + \frac{\Delta c(T^2 - T_{ref}^2)}{2} + \Delta d(T - T_{ref})$$

$$\int_{T_{ref}}^T \frac{\Delta C_p}{T} dT = \frac{\Delta a(T^3 - T_{ref}^3)}{3} + \frac{\Delta b(T^2 - T_{ref}^2)}{2} + \Delta c(T - T_{ref}) + \Delta d \ln \frac{T}{T_{ref}}$$

Where

T is the reaction temperature in K.

T_{ref} is the reference temperature which is 298.15 K.

Estimation of Equilibrium constant:

$$\Delta G_R = -RT \ln K$$

Where

R is the gas constant which is given by $8.315 J.m^3/mol.K$

T is the reaction temperature in K.

K is the equilibrium constant.

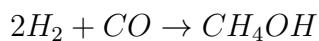
The equilibrium constant K_y for a particular reaction is given by

$$K = K_y * P^{\Delta n}$$

where $\Delta n = \sum_{i=1}^n \vartheta_i$

4.3 Results

The reaction is as follows:



The parameters to the equilibrium reactor is provided as follows:

Basis : Activity

Mode : Isothermal

Phase : Vapour

Rmode : Gibbs

The feed conditions is provided below:

Parameter	Value
Temperature(K)	366.5
Pressure(Pa)	101325
Flow Rate(mol/s)	27.778
Composition	
Hydrogen	0.667
Carbon Monoxide	0.333
Methanol	0

Table 4.1: Feed Conditions

After Simulating the reactor the following results were obtained:

Parameter	DWSIM	OM	Error percentage
Gibbs Energy at 25C(J/mol)	-25170	-25170	0
Conversion			
Hydrogen	74.6635	74.8379	0.233581335
Carbon Monoxide	74.5516	74.9503	0.534797375

Table 4.2: Results

Reference

- Introduction to Chemical Engineering Thermodynamics by Joseph Mauk Smith, Hendrick C. Van Ness, Michael M. Abbott, M. T. Swihart
- Fundamentals of multicomponent distillation by C.D. Holland

Chapter 5

OpenModelica Code

```
1 package DistCol
2 model RaoultLaw
3 //Model Description:
4
5 // The Distillation Column aims to seperate the feed mixture into two
6 // streams i.e. Distillate and Residue based on the Volatility of the
7 // components present in the stream.Multiple Feeds and Side Draws can also
8 // be introduced.
9
10 //Thermodynamics : Raoult Law
11 extends Simulator.Files.Icons.DistillationColumn;
12 //===== User Input Data
13 //=====
14
15 parameter Simulator.Files.ChemsepDatabase.GeneralProperties C[Nc] "
16     Component instances array" annotation(
17     Dialog(tab = "Column Specifications", group = "Component Parameters"));
18 parameter Integer Nc "Number of components" annotation(
19     Dialog(tab = "Column Specifications", group = "Component Parameters"));
20 parameter Integer Nt = 4 "Number of stages" annotation(
21     Dialog(tab = "Column Specifications", group = "Calculation Parameters")
22 );
23 parameter Integer Nout = 0 "Number of side draws" annotation(
24     Dialog(tab = "Column Specifications", group = "Calculation Parameters")
25 );
26 parameter Integer Ni = 1 "Number of feed streams" annotation(
27     Dialog(tab = "Column Specifications", group = "Calculation Parameters")
28 );
29 parameter Integer InT_s[Ni] "Feed stage location" annotation(
30     Dialog(tab = "Column Specifications", group = "Calculation Parameters")
31 );
32 parameter Real D(unit="mol/s") "Distillate flow rate" annotation(
33     Dialog(tab = "Column Specifications", group = "Calculation Parameters")
34 );
35 parameter Real RR(unit="--") "Reflux Ratio" annotation(
36     Dialog(tab = "Column Specifications", group = "Calculation Parameters")
37 );
38 parameter Real CondP(unit="Pa") "Condenser Pressure" annotation(
39     Dialog(tab = "Column Specifications", group = "Calculation Parameters")
40 );
41 parameter Real ReboilerP(unit="Pa") "Reboiler Pressure" annotation(
42     Dialog(tab = "Column Specifications", group = "Calculation Parameters")
43 );
```

```

33 parameter Real Tguess(unit="K") "Guess Temperature" annotation(
34 Dialog(tab = "Column Specifications", group = "Calculation Parameters")
35 );
36 parameter Real SideF[Nout](each unit="mol/s")"Side stream flow rate"
37 annotation(  

38 Dialog(tab = "Column Specifications", group = "Calculation Parameters")
39 );
40 parameter Real SidePhase1 = 0"Side stream Phase 0 for None 1 for Liquid
41 and 2 for Vapour" annotation(  

42 Dialog(tab = "Column Specifications", group = "Calculation Parameters")
43 );
44 parameter Real SidePhase2 = 0"Side stream Phase 0 for None 1 for Liquid
45 and 2 for Vapour" annotation(  

46 Dialog(tab = "Column Specifications", group = "Calculation Parameters")
47 );
48 parameter Real SidePhase3 = 0"Side stream Phase 0 for None 1 for Liquid
49 and 2 for Vapour" annotation(  

50 Dialog(tab = "Column Specifications", group = "Calculation Parameters")
51 );
52 parameter Real SidePhase4 = 0"Side stream Phase 0 for None 1 for Liquid
53 and 2 for Vapour" annotation(  

54 Dialog(tab = "Column Specifications", group = "Calculation Parameters")
55 );
56 parameter Real SidePhase5 = 0"Side stream Phase 0 for None 1 for Liquid
57 and 2 for Vapour" annotation(  

58 Dialog(tab = "Column Specifications", group = "Calculation Parameters")
59 );
60 parameter Real SidePhase6 = 0"Side stream Phase 0 for None 1 for Liquid
61 and 2 for Vapour" annotation(  

62 Dialog(tab = "Column Specifications", group = "Calculation Parameters")
63 );
64 parameter Real SidePhase7 = 0"Side stream Phase 0 for None 1 for Liquid
65 and 2 for Vapour" annotation(  

66 Dialog(tab = "Column Specifications", group = "Calculation Parameters")
67 );
68 parameter String Ctype = "Total" "Condenser type: Total or Partial"
69 annotation(  

70 Dialog(tab = "Column Specifications", group = "Calculation Parameters")
71 );
72
73 //===== Distillation Column Variables
74 =====//  

75
76 //===== Connector Variables
77 =====//  

78 Simulator.Files.Interfaces.matConn In[Ni](each Nc = Nc) annotation(  

79 Placement(visible = true, transformation(origin = {-248, -40}, extent
80 = {{-10, -10}, {10, 10}}, rotation = 0), iconTransformation(
81 origin = {-250, 0}, extent = {{-10, -10}, {10, 10}}, rotation =
82 0)));
83 Simulator.Files.Interfaces.matConn Dist(each Nc = Nc) annotation(  

84 Placement(visible = true, transformation(origin = {250, 316}, extent
85 = {{-10, -10}, {10, 10}}, rotation = 0), iconTransformation(
86 origin = {250, 298}, extent = {{-10, -10}, {10, 10}}, rotation =
87 0));
88 Simulator.Files.Interfaces.matConn Bot(each Nc = Nc) annotation(  

89 Placement(visible = true, transformation(origin = {250, -296}, extent
90 = {{-10, -10}, {10, 10}}, rotation = 0), iconTransformation(
91 origin = {252, -300}, extent = {{-10, -10}, {10, 10}}, rotation =
92 0));
93 Simulator.Files.Interfaces.enConn Cduty annotation(  

94 Placement(visible = true, transformation(origin = {246, 590}, extent
95 = {{-10, -10}, {10, 10}}, rotation = 0), iconTransformation(
96

```

```

    origin = {250, 600}, extent = {{-10, -10}, {10, 10}}, rotation =
0));
66 Simulator.Files.Interfaces.enConn Rduty annotation
67     Placement(visible = true, transformation(origin = {252, -588}, extent
= {{-10, -10}, {10, 10}}, rotation = 0), iconTransformation(
origin = {250, -598}, extent = {{-10, -10}, {10, 10}}, rotation =
0));
68 Simulator.Files.Interfaces.matConn Out_s[Nout](each Nc = Nc) annotation
(
69     Placement(visible = true, transformation(origin = {-36, 32}, extent =
{{-10, -10}, {10, 10}}, rotation = 0), iconTransformation(origin
= {-70, 60}, extent = {{-10, -10}, {10, 10}}, rotation = 0)));
70 // =====
71
72 extends Simulator.GuessModels.InitialGuess;
73 //=====Model Variables
74
75
76
77
78
79
80
81
82
83
84
85
86
87
88
89
90
91
92
93
94
95
96
97
98
99
100
101
102
103
104
105
106
107
//
```

```

108     Real xdel[Nc-1];
109     Real a11,a12,a13,a14,a15,a16,a17,a18,a19,a10;
110     Real xvapin[Ni];
111     Real pervap[Nt];
112     Integer b11;
113     Integer b12,b13,b14,b15,b16,b17;
114 equation
115
116 //===== Pressure at Each Stage


---


117
118 // Pressure at each stage is calculated by interpolation.
119 P[1]=CondP;
120 P[Nt]=ReboilerP;
121 for i in 2:Nt-1 loop
122   if CondP == ReboilerP then
123     P[i]=CondP;
124   else
125     if ReboilerP > CondP then
126       P[i]=CondP + ((i - 1)/(Nt - 1))*(ReboilerP -CondP);
127     else
128       P[i]=CondP + ((i - 1)/(Nt - 1))*(CondP -ReboilerP);
129     end if;
130   end if;
131 end for;
132 //


---


134
135 //=====Determining the Location of the Feed and the Side
136   Stream=====
137   if 1==Ni then
138     a11=InT_s[1]+1;
139     a12=0;
140     a13=0;
141     a14=0;
142     a15=0;
143     a16=0;
144     a17=0;
145     a18=0;
146     a19=0;
147   elseif 2==Ni then
148     a11=InT_s[1]+1;
149     a12=InT_s[2]+1;
150     a13=0;
151     a14=0;
152     a15=0;
153     a16=0;
154     a17=0;
155     a18=0;
156     a19=0;
157     a10=0;
158   elseif 3==Ni then
159     a11=InT_s[1]+1;
160     a12=InT_s[2]+1;
161     a13=InT_s[3]+1;
162     a14=0;
163     a15=0;
164     a16=0;
165     a17=0;

```

```

166     a18=0;
167     a19=0;
168     a10=0;
169 elseif 4==Ni then
170     a11=InT_s[1]+1;
171     a12=InT_s[2]+1;
172     a13=InT_s[3]+1;
173     a14=InT_s[4]+1;
174     a15=0;
175     a16=0;
176     a17=0;
177     a18=0;
178     a19=0;
179     a10=0;
180 elseif 5==Ni then
181     a11=InT_s[1]+1;
182     a12=InT_s[2]+1;
183     a13=InT_s[3]+1;
184     a14=InT_s[4]+1;
185     a15=InT_s[5]+1;
186     a16=0;
187     a17=0;
188     a18=0;
189     a19=0;
190     a10=0;
191 elseif 6==Ni then
192     a11=InT_s[1]+1;
193     a12=InT_s[2]+1;
194     a13=InT_s[3]+1;
195     a14=InT_s[4]+1;
196     a15=InT_s[5]+1;
197     a16=InT_s[6]+1;
198     a17=0;
199     a18=0;
200     a19=0;
201     a10=0;
202 elseif 7==Ni then
203     a11=InT_s[1]+1;
204     a12=InT_s[2]+1;
205     a13=InT_s[3]+1;
206     a14=InT_s[4]+1;
207     a15=InT_s[5]+1;
208     a16=InT_s[6]+1;
209     a17=InT_s[7]+1;
210     a18=0;
211     a19=0;
212     a10=0;
213 elseif 8==Ni then
214     a11=InT_s[1]+1;
215     a12=InT_s[2]+1;
216     a13=InT_s[3]+1;
217     a14=InT_s[4]+1;
218     a15=InT_s[5]+1;
219     a16=InT_s[6]+1;
220     a17=InT_s[7]+1;
221     a18=InT_s[8]+1;
222     a19=0;
223     a10=0;
224 elseif 9==Ni then
225     a11=InT_s[1]+1;
226     a12=InT_s[2]+1;
227     a13=InT_s[3]+1;
228     a14=InT_s[4]+1;
229     a15=InT_s[5]+1;

```

```

230     a16=InT_s[6]+1;
231     a17=InT_s[7]+1;
232     a18=InT_s[8]+1;
233     a19=InT_s[9]+1;
234     a10=0;
235 else
236     a11=InT_s[1]+1;
237     a12=InT_s[2]+1;
238     a13=InT_s[3]+1;
239     a14=InT_s[4]+1;
240     a15=InT_s[5]+1;
241     a16=InT_s[6]+1;
242     a17=InT_s[7]+1;
243     a18=InT_s[8]+1;
244     a19=InT_s[9]+1;
245     a10=InT_s[10]+1;
246 end if;
247 if 1==Nout then
248     b11=OutT_s[1]+1;
249     b12=0;
250     b13=0;
251     b14=0;
252     b15=0;
253     b16=0;
254     b17=0;
255 elseif 2==Nout then
256     b11=OutT_s[1]+1;
257     b12=OutT_s[2]+1;
258     b13=0;
259     b14=0;
260     b15=0;
261     b16=0;
262     b17=0;
263 elseif 3==Nout then
264     b11=OutT_s[1]+1;
265     b12=OutT_s[2]+1;
266     b13=OutT_s[3]+1;
267     b14=0;
268     b15=0;
269     b16=0;
270     b17=0;
271 elseif 4==Nout then
272     b11=OutT_s[1]+1;
273     b12=OutT_s[2]+1;
274     b13=OutT_s[3]+1;
275     b14=OutT_s[4]+1;
276     b15=0;
277     b16=0;
278     b17=0;
279 elseif 5==Nout then
280     b11=OutT_s[1]+1;
281     b12=OutT_s[2]+1;
282     b13=OutT_s[3]+1;
283     b14=OutT_s[4]+1;
284     b15=OutT_s[5]+1;
285     b16=0;
286     b17=0;
287 elseif 6==Nout then
288     b11=OutT_s[1]+1;
289     b12=OutT_s[2]+1;
290     b13=OutT_s[3]+1;
291     b14=OutT_s[4]+1;
292     b16=OutT_s[6]+1;
293     b15=0;

```

```

294     b17=0;
295 elseif 7==Nout then
296     b11=OutT_s[1]+1;
297     b12=OutT_s[2]+1;
298     b13=OutT_s[3]+1;
299     b14=OutT_s[4]+1;
300     b15=OutT_s[5]+1;
301     b16=OutT_s[6]+1;
302     b17=OutT_s[7]+1;
303 else
304     b11=0;
305     b12=0;
306     b13=0;
307     b14=0;
308     b15=0;
309     b16=0;
310     b17=0;
311 end if;
312 //
```

```

313 //=====Determining the Feed Flow Rate at each stage
314 //If the Feed is entering that particular stage it will be assigned the
315 //inlet flow rate else it will be assigned the value zero. If a side
316 //stream is leaving from a particular tray provided that the phase is
317 //liquid it will be assigned the value provided by the user.
318
319 for i in 1:Nt loop
320     if i==a11 then
321         Feed[i]=Fin[1];
322     elseif i==a12 then
323         Feed[i]=Fin[2];
324     elseif i==a13 then
325         Feed[i]=Fin[3];
326     elseif i==a14 then
327         Feed[i]=Fin[4];
328     elseif i==a15 then
329         Feed[i]=Fin[5];
330     elseif i==a16 then
331         Feed[i]=Fin[6];
332     elseif i==a17 then
333         Feed[i]=Fin[7];
334     elseif i==a18 then
335         Feed[i]=Fin[8];
336     elseif i==a19 then
337         Feed[i]=Fin[9];
338     elseif i==a10 then
339         Feed[i]=Fin[10];
340     elseif i==b11 and SidePhase1 == 1 then
341         Feed[i]=(-1*SideF[1]);
342     elseif i==b12 and SidePhase2 == 1 then
343         Feed[i]=(-1*SideF[2]);
344     elseif i==b13 and SidePhase3 == 1 then
345         Feed[i]=(-1*SideF[3]);
346     elseif i==b14 and SidePhase4 == 1 then
347         Feed[i]=(-1*SideF[4]);
348     elseif i==b15 and SidePhase5 == 1 then
349         Feed[i]=(-1*SideF[5]);
350     elseif i==b16 and SidePhase6 == 1 then
351         Feed[i]=(-1*SideF[6]);
352     elseif i==b17 and SidePhase7 == 1 then
353         Feed[i]=(-1*SideF[7]);
354     else
```

```

352     Feed[ i ]=0;
353     end if;
354 end for;
355 //===== Determining the Percentage Vapour of the Feed entering the
356 // paticular stream
356 for i in 1:Nt loop
357     if i==a11 then
358         pervap[ i]=xvapin[ 1 ];
359     elseif i==a12 then
360         pervap[ i]=xvapin[ 2 ];
361     elseif i==a13 then
362         pervap[ i]=xvapin[ 3 ];
363     elseif i==a14 then
364         pervap[ i]=xvapin[ 4 ];
365     elseif i==a15 then
366         pervap[ i]=xvapin[ 5 ];
367     elseif i==a16 then
368         pervap[ i]=xvapin[ 6 ];
369     elseif i==a17 then
370         pervap[ i]=xvapin[ 7 ];
371     elseif i==a18 then
372         pervap[ i]=xvapin[ 8 ];
373     elseif i==a19 then
374         pervap[ i]=xvapin[ 9 ];
375     elseif i==a10 then
376         pervap[ i]=xvapin[ 10 ];
377     else
378         pervap[ i]=0;
379     end if;
380 end for;
381 for i in 1:Nc loop
382     Fc[ 1 , i ]=0;
383 end for;
384 //
385 //=====Overall Material Balance
386 if Nout > 0 then
387     sum( Fin [ : ] )=B+D+sum( SideF [ : ] );
388 else
389     sum( Fin [ : ] )=B+D;
390 end if;
391 //
392 // connector equations
393 for i in 1:Ni loop
394     In[ i ].P = Pin[ i ];
395     In[ i ].T = Tin[ i ];
396     In[ i ].H = Hin[ i ];
397     In[ i ].F = Fin[ i ];
398     In[ i ].x_pc[ 1 , : ] = x_c[ i , : ];
399     In[ i ].xvap=xvapin[ i ];
400 end for;
401 Dist.P = CondP;
402 Dist.T = T[ 1 ];
403 Dist.F = D;
404 Dist.H = Hout1;
405 Dist.x_pc[ 1 , : ] = ( integer(x[ 1 , : ] .*10000) ./10000;
406 Bot.P = P[ Nt ];
407 Bot.T = T[ Nt ];
408 Bot.F = B;
409 Bot.H = Hout2;

```

```

410 Bot.x_pc [1, :] = (integer(x[Nt,:]*10000) ./10000;
411 Cduty.Q=Qc;
412 Rduty.Q=Qr;
413 // _____
414 //===== At Condenser
415 V[1]=L[1]+D;
416 RR=L[1]/D;
417 for i in 1:Nc loop
418     Pvap_c[1,i] = Simulator.Files.ThermodynamicFunctions.Psat(C[i].VP, T[1]);
419 end for;
420 for j in 1:Nc loop
421     K_c[1,j] = Pvap_c[1,j] / P[1];
422 end for;
423 sum(x[1,:]*K_c[1,:])=1;//Bubble Point Equation
424 // _____
425 //=====Assumption For Vapor Flow : Equimolar Flow
426 for k in 2:Nt+1 loop
427     if Nout > 0 and SidePhase1 == 2 and k== b11 then
428         V[k]=V[k-1]-SideF[1];
429     elseif Nout > 0 and SidePhase2 == 2 and k== b12 then
430         V[k]=V[k-1]-SideF[2];
431     elseif Nout > 0 and SidePhase3 == 2 and k== b13 then
432         V[k]=V[k-1]-SideF[3];
433     elseif Nout > 0 and SidePhase4 == 2 and k== b14 then
434         V[k]=V[k-1]-SideF[4];
435     elseif Nout > 0 and SidePhase5 == 2 and k== b15 then
436         V[k]=V[k-1]-SideF[5];
437     elseif Nout > 0 and SidePhase6 == 2 and k== b16 then
438         V[k]=V[k-1]-SideF[6];
439     elseif Nout > 0 and SidePhase7 == 2 and k== b17 then
440         V[k]=V[k-1]-SideF[7];
441     else
442         V[k]=V[k-1]+(Feed[k-1]*pervap[k-1]);
443     end if;
444 end for;
445 // _____
446 //=====Calculation of Vapour Composition at Condenser and 1st
447 Stage=====
447 y[1,:]=x[1,:]*K_c[1,:];
448 sum(y[2,:])=1;
449 for i in 1:Nc-1 loop
450     y[2,i]=x[1,i];
451 end for;
452 // _____
453 //=====Calculation from 2nd Stage to Reboiler
454
455 for m in 2:Nt loop
456 //Liquid Flow Rate at the paticular stage calculated from material balance
457 //at that stage
457 if m==Nt then
458     L[m]=B;
459 else

```

```

460     L[m]=(Feed[m]*(1-pervap[m]))+L[m-1];
461 end if;
462 //

---


463 //Thermodynamic Calculation at that Stage
464 for n in 1:Nc loop
465     Pvap_c[m,n] = Simulator.Files.ThermodynamicFunctions.Psat(C[n].VP, T[
466     m]);
467 end for;
468 for p in 1:Nc loop
469     K_c[m,p] = Pvap_c[m,p] / P[m];
470 end for;
471 for q in 1:Nc loop
472     y[m,q]-(x[m,q]*K_c[m,q])=0;
473 end for;
474 sum(x[m,:])=1;
475 // Assigning the Inlet Component Flow Rates and Leaving Side Streams
476     Component Flow Rates
477 if m==a11 then
478     for k in 1:Nc loop
479         Fc[m,k]=Fin[1]*x_c[1,k];
480     end for;
481 elseif m==a12 then
482     for k in 1:Nc loop
483         Fc[m,k]=Fin[2]*x_c[2,k];
484     end for;
485 elseif m==a13 then
486     for k in 1:Nc loop
487         Fc[m,k]=Fin[3]*x_c[3,k];
488     end for;
489 elseif m==a14 then
490     for k in 1:Nc loop
491         Fc[m,k]=Fin[4]*x_c[4,k];
492     end for;
493 elseif m==a15 then
494     for k in 1:Nc loop
495         Fc[m,k]=Fin[5]*x_c[5,k];
496     end for;
497 elseif m==a16 then
498     for k in 1:Nc loop
499         Fc[m,k]=Fin[6]*x_c[6,k];
500     end for;
501 elseif m==a17 then
502     for k in 1:Nc loop
503         Fc[m,k]=Fin[7]*x_c[7,k];
504     end for;
505 elseif m==a18 then
506     for k in 1:Nc loop
507         Fc[m,k]=Fin[8]*x_c[8,k];
508     end for;
509 elseif m==a19 then
510     for k in 1:Nc loop
511         Fc[m,k]=Fin[9]*x_c[9,k];
512     end for;
513 elseif m==a10 then
514     for k in 1:Nc loop
515         Fc[m,k]=Fin[10]*x_c[10,k];
516     end for;
517 elseif m==b11 then
518     if SidePhase1==2 then
519         for k in 1:Nc loop
520             Fc[m,k]=(-1*SideF[1]*y[m,k]);
521         end for;

```

```

520     else
521         for k in 1:Nc loop
522             Fc[m,k]=(-1*SideF[1]*x[m,k]) ;
523         end for;
524     end if;
525 elseif m==b12 then
526     if SidePhase2==2 then
527         for k in 1:Nc loop
528             Fc[m,k]=(-1*SideF[2]*y[m,k]) ;
529         end for;
530     else
531         for k in 1:Nc loop
532             Fc[m,k]=(-1*SideF[2]*x[m,k]) ;
533         end for;
534     end if;
535 elseif m==b13 then
536     if SidePhase3==2 then
537         for k in 1:Nc loop
538             Fc[m,k]=(-1*SideF[3]*y[m,k]) ;
539         end for;
540     else
541         for k in 1:Nc loop
542             Fc[m,k]=(-1*SideF[3]*x[m,k]) ;
543         end for;
544     end if;
545 elseif m==b14 then
546     if SidePhase4==2 then
547         for k in 1:Nc loop
548             Fc[m,k]=(-1*SideF[4]*y[m,k]) ;
549         end for;
550     else
551         for k in 1:Nc loop
552             Fc[m,k]=(-1*SideF[4]*x[m,k]) ;
553         end for;
554     end if;
555 elseif m==b15 then
556     if SidePhase5==2 then
557         for k in 1:Nc loop
558             Fc[m,k]=(-1*SideF[5]*y[m,k]) ;
559         end for;
560     else
561         for k in 1:Nc loop
562             Fc[m,k]=(-1*SideF[5]*x[m,k]) ;
563         end for;
564     end if;
565 elseif m==b16 then
566     if SidePhase6==2 then
567         for k in 1:Nc loop
568             Fc[m,k]=(-1*SideF[6]*y[m,k]) ;
569         end for;
570     else
571         for k in 1:Nc loop
572             Fc[m,k]=(-1*SideF[6]*x[m,k]) ;
573         end for;
574     end if;
575 elseif m==b17 then
576     if SidePhase7==2 then
577         for k in 1:Nc loop
578             Fc[m,k]=(-1*SideF[7]*y[m,k]) ;
579         end for;
580     else
581         for k in 1:Nc loop
582             Fc[m,k]=(-1*SideF[7]*x[m,k]) ;
583         end for;

```

```

584     end if;
585 else
586     for l in 1:Nc loop
587         Fc[m,l]=0;
588     end for;
589     end if;
590     // =====
591 //=====Calculating the Composition of Vapour Flow Rate Entering the
592 Stage=====
593 for r in 1:Nc-1 loop
594     if (((V[m]*y[m,r])+(L[m]*x[m,r])-Fc[m,r]-(L[m-1]*x[m-1,r]))/V[m+1]) < 0
595         or (((V[m]*y[m,r])+(L[m]*x[m,r])-Fc[m,r]-(L[m-1]*x[m-1,r]))/V[m
596         +1]) > 1 then
597         y[m+1,r]=y[m,r];
598     else
599         (L[m-1]*x[m-1,r]) + (V[m+1]*y[m+1,r])+ Fc[m,r]-(V[m]*y[m,r])- (L[m]*x[
600             m,r])=0;
601     end if;
602 end for;
603 sum(y[m+1,:])=1;
604 end for;
605 //=====
606 // Conditions:
607 // Assigning the Condition that the difference between the reboiler
608 // composition from the calculated value and the obtained value should
609 // be zero.
610 for h in 1:Nc-1 loop
611     xdel[h]=((sum(Fc[:,h]))-(D*x[1,h]))/B;
612 end for;
613 for w in 1:Nc-1 loop
614     x[Nt,w]-xdel[w]=0;
615 end for;
616 sum(x[1,:])=1;
617 // =====
618 //=====Energy Balance Calculation
619 for i in 1:Nc loop
620     Hvapcond_c[i] = Simulator.Files.ThermodynamicFunctions.HVapId(C[i].SH,
621                 C[i].VapCp, C[i].HOV, C[i].Tc, T[2]);
622     Hliqcond_c[i] = Simulator.Files.ThermodynamicFunctions.HLiqId(C[i].SH,
623                 C[i].VapCp, C[i].HOV, C[i].Tc, T[1]);
624 end for;
625 if Ctype == "Total" then
626     Hliqcond = Hout1;
627 elseif Ctype == "Partial" then
628     Hliqcond = sum(y[2,:].* Hliqcond_c[:]);
629 end if;
630 Hvapcond = sum(y[2,:].* Hvapcond_c[:]);
631 if Nout > 0 then
632     sum(Fin[:,]* Hin[:,]) + Qr - Qc = B * Hout2 + D * Hliqcond + sum(SideF
633     [:].* HSideOut[:]);
634 else
635     sum(Fin[:,]* Hin[:,]) - Qr = B * Hout2 + D * Hliqcond + Qc;
636 end if;
637 V[1] * Hvapcond = Qc + D * Hliqcond + L[1] * Hout1;
638 //==Assigning the Obtained Values to the Side Streams if Selected
639 if Nout == 1 then
640     Out_s[1].P = P[b11];
641     Out_s[1].T = T[b11];

```

```

633 Out_s[1].F = (-1*Feed[b11]);  

634 Out_s[1].H= HSideOut[1];  

635 if SidePhase1==1 then  

636     Out_s[1].x_pc[1, :] = (integer(x[b11,:]*10000)) ./10000;  

637 else  

638     Out_s[1].x_pc[1, :] = (integer(y[b11,:]*10000)) ./10000;  

639 end if;  

640 end if;  

641 if Nout==2 then  

642     Out_s[1].P = P[b11];  

643     Out_s[1].T = T[b11];  

644     Out_s[1].F = (-1*Feed[b11]);  

645     Out_s[1].H= HSideOut[1];  

646     if SidePhase1==1 then  

647         Out_s[1].x_pc[1, :] = (integer(x[b11,:]*10000)) ./10000;  

648     else  

649         Out_s[1].x_pc[1, :] = (integer(y[b11,:]*10000)) ./10000;  

650     end if;  

651     Out_s[2].P = P[b12];  

652     Out_s[2].T = T[b12];  

653     Out_s[2].F = (-1*Feed[b12]);  

654     Out_s[2].H= HSideOut[2];  

655     if SidePhase2==1 then  

656         Out_s[2].x_pc[1, :] = (integer(x[b12,:]*10000)) ./10000;  

657     else  

658         Out_s[2].x_pc[1, :] = (integer(y[b12,:]*10000)) ./10000;  

659     end if;  

660 end if;  

661 if Nout==3 then  

662     Out_s[1].P = P[b11];  

663     Out_s[1].T = T[b11];  

664     Out_s[1].F = (-1*Feed[b11]);  

665     Out_s[1].H= HSideOut[1];  

666     if SidePhase1==1 then  

667         Out_s[1].x_pc[1, :] = (integer(x[b11,:]*10000)) ./10000;  

668     else  

669         Out_s[1].x_pc[1, :] = (integer(y[b11,:]*10000)) ./10000;  

670     end if;  

671     Out_s[2].P = P[b12];  

672     Out_s[2].T = T[b12];  

673     Out_s[2].F = (-1*Feed[b12]);  

674     Out_s[2].H= HSideOut[2];  

675     if SidePhase2==1 then  

676         Out_s[2].x_pc[1, :] = (integer(x[b12,:]*10000)) ./10000;  

677     else  

678         Out_s[2].x_pc[1, :] = (integer(y[b12,:]*10000)) ./10000;  

679     end if;  

680     Out_s[3].P = P[b13];  

681     Out_s[3].T = T[b13];  

682     Out_s[3].F = (-1*Feed[b13]);  

683     Out_s[3].H= HSideOut[3];  

684     if SidePhase3==1 then  

685         Out_s[3].x_pc[1, :] = (integer(x[b13,:]*10000)) ./10000;  

686     else  

687         Out_s[3].x_pc[1, :] = (integer(y[b13,:]*10000)) ./10000;  

688     end if;  

689 end if;  

690 if Nout==4 then  

691     Out_s[1].P = P[b11];  

692     Out_s[1].T = T[b11];  

693     Out_s[1].F = (-1*Feed[b11]);  

694     Out_s[1].H= HSideOut[1];  

695     if SidePhase1==1 then  

696         Out_s[1].x_pc[1, :] = (integer(x[b11,:]*10000)) ./10000;

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```

697     else
698         Out_s[1].x_pc[1, :] = (integer(y[b11,:]*10000)) ./10000;
699     end if;
700     Out_s[2].P = P[b12];
701     Out_s[2].T = T[b12];
702     Out_s[2].F = (-1*Feed[b12]);
703     Out_s[2].H= HSideOut[2];
704     if SidePhase2==1 then
705         Out_s[2].x_pc[1, :] = (integer(x[b12,:]*10000)) ./10000;
706     else
707         Out_s[2].x_pc[1, :] = (integer(y[b12,:]*10000)) ./10000;
708     end if;
709     Out_s[3].P = P[b13];
710     Out_s[3].T = T[b13];
711     Out_s[3].F = (-1*Feed[b13]);
712     Out_s[3].H= HSideOut[3];
713     if SidePhase3==1 then
714         Out_s[3].x_pc[1, :] = (integer(x[b13,:]*10000)) ./10000;
715     else
716         Out_s[3].x_pc[1, :] = (integer(y[b13,:]*10000)) ./10000;
717     end if;
718     Out_s[4].P = P[b14];
719     Out_s[4].T = T[b14];
720     Out_s[4].F = (-1*Feed[b12]);
721     Out_s[4].H= HSideOut[4];
722     if SidePhase4==1 then
723         Out_s[4].x_pc[1, :] = (integer(x[b14,:]*10000)) ./10000;
724     else
725         Out_s[4].x_pc[1, :] = (integer(y[b14,:]*10000)) ./10000;
726     end if;
727 end if;
728 if Nout ==5 then
729     Out_s[1].P = P[b11];
730     Out_s[1].T = T[b11];
731     Out_s[1].F = (-1*Feed[b11]);
732     Out_s[1].H= HSideOut[1];
733     if SidePhase1==1 then
734         Out_s[1].x_pc[1, :] = (integer(x[b11,:]*10000)) ./10000;
735     else
736         Out_s[1].x_pc[1, :] = (integer(y[b11,:]*10000)) ./10000;
737     end if;
738     Out_s[2].P = P[b12];
739     Out_s[2].T = T[b12];
740     Out_s[2].F = (-1*Feed[b12]);
741     Out_s[2].H= HSideOut[2];
742     if SidePhase2==1 then
743         Out_s[2].x_pc[1, :] = (integer(x[b12,:]*10000)) ./10000;
744     else
745         Out_s[2].x_pc[1, :] = (integer(y[b12,:]*10000)) ./10000;
746     end if;
747     Out_s[3].P = P[b13];
748     Out_s[3].T = T[b13];
749     Out_s[3].F = (-1*Feed[b13]);
750     Out_s[3].H= HSideOut[3];
751     if SidePhase3==1 then
752         Out_s[3].x_pc[1, :] = (integer(x[b13,:]*10000)) ./10000;
753     else
754         Out_s[3].x_pc[1, :] = (integer(y[b13,:]*10000)) ./10000;
755     end if;
756     Out_s[4].P = P[b14];
757     Out_s[4].T = T[b14];
758     Out_s[4].F = (-1*Feed[b12]);
759     Out_s[4].H= HSideOut[4];
760     if SidePhase4==1 then

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761     Out_s[4].x_pc[1, :] = (integer(x[b14,:]*10000)) ./10000;
762   else
763     Out_s[4].x_pc[1, :] = (integer(y[b14,:]*10000)) ./10000;
764   end if;
765   Out_s[5].P = P[b15];
766   Out_s[5].T = T[b15];
767   Out_s[5].F = (-1*Feed[b15]);
768   Out_s[5].H= HSideOut[5];
769   if SidePhase5==1 then
770     Out_s[5].x_pc[1, :] = (integer(x[b12,:]*10000)) ./10000;
771   else
772     Out_s[5].x_pc[1, :] = (integer(y[b12,:]*10000)) ./10000;
773   end if;
774 end if;
775 if Nout==6 then
776   Out_s[1].P = P[b11];
777   Out_s[1].T = T[b11];
778   Out_s[1].F = (-1*Feed[b11]);
779   Out_s[1].H= HSideOut[1];
780   if SidePhase1==1 then
781     Out_s[1].x_pc[1, :] = (integer(x[b11,:]*10000)) ./10000;
782   else
783     Out_s[1].x_pc[1, :] = (integer(y[b11,:]*10000)) ./10000;
784   end if;
785   Out_s[2].P = P[b12];
786   Out_s[2].T = T[b12];
787   Out_s[2].F = (-1*Feed[b12]);
788   Out_s[2].H= HSideOut[2];
789   if SidePhase2==1 then
790     Out_s[2].x_pc[1, :] = (integer(x[b12,:]*10000)) ./10000;
791   else
792     Out_s[2].x_pc[1, :] = (integer(y[b12,:]*10000)) ./10000;
793   end if;
794   Out_s[3].P = P[b13];
795   Out_s[3].T = T[b13];
796   Out_s[3].F = (-1*Feed[b13]);
797   Out_s[3].H= HSideOut[3];
798   if SidePhase3==1 then
799     Out_s[3].x_pc[1, :] = (integer(x[b13,:]*10000)) ./10000;
800   else
801     Out_s[3].x_pc[1, :] = (integer(y[b13,:]*10000)) ./10000;
802   end if;
803   Out_s[4].P = P[b14];
804   Out_s[4].T = T[b14];
805   Out_s[4].F = (-1*Feed[b12]);
806   Out_s[4].H= HSideOut[4];
807   if SidePhase4==1 then
808     Out_s[4].x_pc[1, :] = (integer(x[b14,:]*10000)) ./10000;
809   else
810     Out_s[4].x_pc[1, :] = (integer(y[b14,:]*10000)) ./10000;
811   end if;
812   Out_s[5].P = P[b15];
813   Out_s[5].T = T[b15];
814   Out_s[5].F = (-1*Feed[b15]);
815   Out_s[5].H= HSideOut[5];
816   if SidePhase5==1 then
817     Out_s[5].x_pc[1, :] = (integer(x[b12,:]*10000)) ./10000;
818   else
819     Out_s[5].x_pc[1, :] = (integer(y[b12,:]*10000)) ./10000;
820   end if;
821   Out_s[6].P = P[b16];
822   Out_s[6].T = T[b16];
823   Out_s[6].F = (-1*Feed[b16]);
824   Out_s[6].H= HSideOut[6];

```

```

825   if SidePhase6==1 then
826     Out_s[6].x_pc[1, :] = (integer(x[b16,:]*10000)) ./10000;
827   else
828     Out_s[6].x_pc[1, :] = (integer(y[b16,:]*10000)) ./10000;
829   end if;
830 end if;
831   if Nout==7 then
832     Out_s[1].P = P[b11];
833     Out_s[1].T = T[b11];
834     Out_s[1].F = (-1*Feed[b11]);
835     Out_s[1].H= HSideOut[1];
836     if SidePhase1==1 then
837       Out_s[1].x_pc[1, :] = (integer(x[b11,:]*10000)) ./10000;
838     else
839       Out_s[1].x_pc[1, :] = (integer(y[b11,:]*10000)) ./10000;
840     end if;
841     Out_s[2].P = P[b12];
842     Out_s[2].T = T[b12];
843     Out_s[2].F = (-1*Feed[b12]);
844     Out_s[2].H= HSideOut[2];
845     if SidePhase2==1 then
846       Out_s[2].x_pc[1, :] = (integer(x[b12,:]*10000)) ./10000;
847     else
848       Out_s[2].x_pc[1, :] = (integer(y[b12,:]*10000)) ./10000;
849     end if;
850     Out_s[3].P = P[b13];
851     Out_s[3].T = T[b13];
852     Out_s[3].F = (-1*Feed[b13]);
853     Out_s[3].H= HSideOut[3];
854     if SidePhase3==1 then
855       Out_s[3].x_pc[1, :] = (integer(x[b13,:]*10000)) ./10000;
856     else
857       Out_s[3].x_pc[1, :] = (integer(y[b13,:]*10000)) ./10000;
858     end if;
859     Out_s[4].P = P[b14];
860     Out_s[4].T = T[b14];
861     Out_s[4].F = (-1*Feed[b12]);
862     Out_s[4].H= HSideOut[4];
863     if SidePhase4==1 then
864       Out_s[4].x_pc[1, :] = (integer(x[b14,:]*10000)) ./10000;
865     else
866       Out_s[4].x_pc[1, :] = (integer(y[b14,:]*10000)) ./10000;
867     end if;
868     Out_s[5].P = P[b15];
869     Out_s[5].T = T[b15];
870     Out_s[5].F = (-1*Feed[b15]);
871     Out_s[5].H= HSideOut[5];
872     if SidePhase5==1 then
873       Out_s[5].x_pc[1, :] = (integer(x[b12,:]*10000)) ./10000;
874     else
875       Out_s[5].x_pc[1, :] = (integer(y[b12,:]*10000)) ./10000;
876     end if;
877     Out_s[6].P = P[b16];
878     Out_s[6].T = T[b16];
879     Out_s[6].F = (-1*Feed[b16]);
880     Out_s[6].H= HSideOut[6];
881     if SidePhase6==1 then
882       Out_s[6].x_pc[1, :] = (integer(x[b16,:]*10000)) ./10000;
883     else
884       Out_s[6].x_pc[1, :] = (integer(y[b16,:]*10000)) ./10000;
885     end if;
886     Out_s[7].P = P[b17];
887     Out_s[7].T = T[b17];
888     Out_s[7].F = (-1*Feed[b12]);

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```

889     Out_s[ 7 ].H= HSideOut [ 7 ];
890     if SidePhase7==1 then
891         Out_s[ 7 ].x_pc[ 1, : ] = ( integer(x[ b17, : ] .*10000) ) ./10000;
892     else
893         Out_s[ 7 ].x_pc[ 1, : ] = ( integer(y[ b17, : ] .*10000) ) ./10000;
894     end if;
895     end if;
896 //===== Correct Flow Rates through Energy Balance
897 for i in 1:Nt loop
898     if i==a11 then
899         HFeed[ i ]=Hin[ 1 ];
900         F[ i ]=Fin[ 1 ];
901     elseif i==a12 then
902         HFeed[ i ]=Hin[ 2 ];
903         F[ i ]=Fin[ 2 ];
904     elseif i==a13 then
905         HFeed[ i ]=Hin[ 3 ];
906         F[ i ]=Fin[ 3 ];
907     elseif i==a14 then
908         HFeed[ i ]=Hin[ 4 ];
909         F[ i ]=Fin[ 4 ];
910     elseif i==a15 then
911         HFeed[ i ]=Hin[ 5 ];
912         F[ i ]=Fin[ 5 ];
913     elseif i==a16 then
914         HFeed[ i ]=Hin[ 6 ];
915         F[ i ]=Fin[ 6 ];
916     elseif i==a17 then
917         HFeed[ i ]=Hin[ 7 ];
918         F[ i ]=Fin[ 7 ];
919     elseif i==a18 then
920         HFeed[ i ]=Hin[ 8 ];
921         F[ i ]=Fin[ 8 ];
922     elseif i==a19 then
923         HFeed[ i ]=Hin[ 9 ];
924         F[ i ]=Fin[ 9 ];
925     elseif i==a10 then
926         HFeed[ i ]=Hin[ 10 ];
927         F[ i ]=Fin[ 10 ];
928     else
929         HFeed[ i ]=0;
930         F[ i ]=0;
931     end if;
932 end for;
933 for i in 1:Nt loop
934     if i==b11 then
935         HSide[ i ]=HSideOut[ 1 ];
936         FSide[ i ]=SideF[ 1 ];
937     elseif i==b12 then
938         HSide[ i ]=HSideOut[ 2 ];
939         FSide[ i ]=SideF[ 2 ];
940     elseif i==b13 then
941         HSide[ i ]=HSideOut[ 3 ];
942         FSide[ i ]=SideF[ 3 ];
943     elseif i==b14 then
944         HSide[ i ]=HSideOut[ 4 ];
945         FSide[ i ]=SideF[ 4 ];
946     elseif i==b15 then
947         HSide[ i ]=HSideOut[ 5 ];
948         FSide[ i ]=SideF[ 5 ];
949     elseif i==b16 then
950         HSide[ i ]=HSideOut[ 6 ];
951         FSide[ i ]=SideF[ 6 ];
952     elseif i==b17 then

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953     HSide[ i]=HSideOut[ 7];
954     FSide[ i]=SideF[ 7];
955     else
956     HSide[ i]=0;
957     FSide[ i]=0;
958     end if;
959     end for;
960 for j in 1:Nt loop
961   for i in 1:Nc loop
962     Hvap[ j,i ] = Simulator.Files.ThermodynamicFunctions.HVapId(C[ i ].SH, C[ i ]
963       ].VapCp, C[ i ].HOV, C[ i ].Tc, T[ j ] );
964     Hliq[ j,i ] = Simulator.Files.ThermodynamicFunctions.HLiqId(C[ i ].SH, C[ i ]
965       ].VapCp, C[ i ].HOV, C[ i ].Tc, T[ j ] );
966   end for;
967   end for;
968   correctL[ 1]=L[ 1 ];
969   correctV[ 1]=0;
970   correctV[ 2]=V[ 1 ];
971   correctL[ Nt]=B;
972   //=====Energy Balance at each stage
973   for i in 2:Nt-1 loop
974     F[ i ]+correctL[ i-1 ]+correctV[ i+1 ]-correctV[ i ]-correctL[ i ]-FSide[ i ]=0;
975     (F[ i ]*HFeed[ i ]) +(correctL[ i-1 ]*sum(Hliq[ i-1, : ].*x[ i-1, : ])) +(correctV[ i
976       ]+1)*sum(Hvap[ i+1, : ].*y[ i+1, : ])) -(correctV[ i ]*sum(Hvap[ i, : ].*y[ i, : ]))
977     -(correctL[ i ]*sum(Hliq[ i, : ].*x[ i, : ])) -(FSide[ i ]*HSide[ i ])=0;
978   end for;
979   ///
980
981
982 end RaoultLaw;
983 model NRTL
984   //Model Description:
985
986   // The Distillation Column aims to seperate the feed mixture into two
987   // streams i.e. Distillate and Residue based on the Volatility of the
988   // components present in the stream. Multiple Feeds and Side Draws can
989   // also be introduced.
990
991   // Thermodynamics : Raoult Law
992   extends Simulator.Files.Icons.DistillationColumn;
993   //===== User Input Data
994   //=====
995
996   parameter Simulator.Files.ChemsepDatabase.GeneralProperties C[Nc] "
997     Component instances array" annotation(  

998     Dialog(tab = "Column Specifications", group = "Component Parameters")
999     );
1000   parameter Integer Nc "Number of components" annotation(  

1001     Dialog(tab = "Column Specifications", group = "Component Parameters")
1002     );
1003   parameter Integer Nt = 4 "Number of stages" annotation(  

1004     Dialog(tab = "Column Specifications", group = "Calculation Parameters"
1005     ));
1006   parameter Integer Nout = 0 "Number of side draws" annotation(  

1007     Dialog(tab = "Column Specifications", group = "Calculation Parameters"
1008     ));
1009   parameter Integer Ni = 1 "Number of feed streams" annotation(  

1010     Dialog(tab = "Column Specifications", group = "Calculation Parameters"
1011     ));
1012   parameter Integer InT_s[Ni] "Feed stage location" annotation(  

1013     Dialog(tab = "Column Specifications", group = "Calculation Parameters"
1014     ));
1015   parameter Integer OutT_s[Nout] "Feed stage location" annotation(  

1016     Dialog(tab = "Column Specifications", group = "Calculation Parameters"
1017     ));

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999     Dialog(tab = "Column Specifications", group = "Calculation Parameters
      ");
1000    parameter Real D(unit="mol/s") "Distillate flow rate" annotation(  

1001      Dialog(tab = "Column Specifications", group = "Calculation Parameters
      "));
1002    parameter Real RR(unit="--") "Reflux Ratio" annotation(  

1003      Dialog(tab = "Column Specifications", group = "Calculation Parameters
      "));
1004    parameter Real CondP(unit="Pa") "Condenser Pressure" annotation(  

1005      Dialog(tab = "Column Specifications", group = "Calculation Parameters
      "));
1006    parameter Real ReboilerP(unit="Pa") "Reboiler Pressure" annotation(  

1007      Dialog(tab = "Column Specifications", group = "Calculation Parameters
      "));
1008    parameter Real Tguess(unit="K") "Guess Temperature" annotation(  

1009      Dialog(tab = "Column Specifications", group = "Calculation Parameters
      "));
1010   parameter Real SideF[Nout](each unit="mol/s")"Side stream flow rate"
      annotation(  

1011     Dialog(tab = "Column Specifications", group = "Calculation Parameters
      "));
1012   parameter Real SidePhase1 = 0"Side stream Phase 0 for None 1 for
      Liquid and 2 for Vapour" annotation(  

1013     Dialog(tab = "Column Specifications", group = "Calculation Parameters
      "));
1014   parameter Real SidePhase2 = 0"Side stream Phase 0 for None 1 for
      Liquid and 2 for Vapour" annotation(  

1015     Dialog(tab = "Column Specifications", group = "Calculation Parameters
      "));
1016   parameter Real SidePhase3 = 0"Side stream Phase 0 for None 1 for
      Liquid and 2 for Vapour" annotation(  

1017     Dialog(tab = "Column Specifications", group = "Calculation Parameters
      "));
1018   parameter Real SidePhase4 = 0"Side stream Phase 0 for None 1 for
      Liquid and 2 for Vapour" annotation(  

1019     Dialog(tab = "Column Specifications", group = "Calculation Parameters
      "));
1020   parameter Real SidePhase5 = 0"Side stream Phase 0 for None 1 for
      Liquid and 2 for Vapour" annotation(  

1021     Dialog(tab = "Column Specifications", group = "Calculation Parameters
      "));
1022   parameter Real SidePhase6 = 0"Side stream Phase 0 for None 1 for
      Liquid and 2 for Vapour" annotation(  

1023     Dialog(tab = "Column Specifications", group = "Calculation Parameters
      "));
1024   parameter Real SidePhase7 = 0"Side stream Phase 0 for None 1 for
      Liquid and 2 for Vapour" annotation(  

1025     Dialog(tab = "Column Specifications", group = "Calculation Parameters
      "));
1026   parameter String Ctype = "Total" "Condenser type: Total or Partial"
      annotation(  

1027     Dialog(tab = "Column Specifications", group = "Calculation Parameters
      "));
1028
1029
1030 //===== Distillation Column Variables
1031 //=====
1032 //===== Connector Variables
1033 //=====
1034 Simulator.Files.Interfaces.matConn In[Ni](each Nc = Nc) annotation(  

      Placement(visible = true, transformation(origin = {-248, -40},  

        extent = {{-10, -10}, {10, 10}}, rotation = 0),  

        iconTransformation(origin = {-250, 0}, extent = {{-10, -10},

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1035           {10, 10}}, rotation = 0)));
1036 Simulator.Files.Interfaces.matConn Dist(each Nc = Nc) annotation(  

1037     Placement(visible = true, transformation(origin = {250, 316},  

1038         extent = {{-10, -10}, {10, 10}}, rotation = 0),  

1039         iconTransformation(origin = {250, 298}, extent = {{-10, -10},  

1040             {10, 10}}, rotation = 0)));
1041 Simulator.Files.Interfaces.matConn Bot(each Nc = Nc) annotation(  

1042     Placement(visible = true, transformation(origin = {250, -296},  

1043         extent = {{-10, -10}, {10, 10}}, rotation = 0),  

1044         iconTransformation(origin = {252, -300}, extent = {{-10, -10},  

1045             {10, 10}}, rotation = 0)));
1046 Simulator.Files.Interfaces.enConn Cduty annotation(  

1047     Placement(visible = true, transformation(origin = {246, 590},  

1048         extent = {{-10, -10}, {10, 10}}, rotation = 0),  

1049         iconTransformation(origin = {250, 600}, extent = {{-10, -10},  

1050             {10, 10}}, rotation = 0)));
1051 Simulator.Files.Interfaces.enConn Rduty annotation(  

1052     Placement(visible = true, transformation(origin = {252, -588},  

1053         extent = {{-10, -10}, {10, 10}}, rotation = 0),  

1054         iconTransformation(origin = {250, -598}, extent = {{-10, -10},  

1055             {10, 10}}, rotation = 0)));
1056 Simulator.Files.Interfaces.matConn Out_s[Nout](each Nc = Nc)  

1057     annotation(  

1058         Placement(visible = true, transformation(origin = {-36, 32}, extent  

1059             = {{-10, -10}, {10, 10}}, rotation = 0), iconTransformation(  

1060                 origin = {-70, 60}, extent = {{-10, -10}, {10, 10}}, rotation =  

1061                 0)));
1062 //
```

```

1046 extends Simulator.GuessModels.InitialGuess;  

1047 //=====Model Variables  

1048  

1049     Real Qc(unit="W") "Condenser Duty";  

1050     Real Qr(unit="W") "Reboiler Duty";  

1051     Real Hvapcond_c[Nc](each unit="J/mol") "Enthalpy of Components present  

1052         in Vapour from Stage 1";  

1053     Real Hliqcond_c[Nc](each unit="J/mol") "Enthalpy of Components present  

1054         in Liquid from Condenser";  

1055     Real Hvapcond(unit="J/mol") "Enthalpy of Vapour from Stage 1";  

1056     Real Hout1(unit="J/mol") "Enthalpy of the Distillate Stream";  

1057     Real Hout2(unit="J/mol") "Enthalpy of the Residue Stream";  

1058     Real Hin[Ni](unit="J/mol") "Enthalpy of the Feed Stream";  

1059     Real Hliqcond(unit="J/mol") "Enthalpy of Vapour from Stage 1";  

1060     Real Fin[Ni](each unit = "mol/s", each min = 0) "Inlet stream molar  

1061         flow rate";  

1062     Real Pin[Ni](each unit = "Pa", each min = 0) "Inlet stream pressure";  

1063     Real Tin[Ni](each unit = "K", each min = 0) "Inlet stream emperature"  

1064         ;  

1065     Real x_c[Ni,Nc](each unit = "-") "Component mole fraction";  

1066     Real Feed[Nt](each unit="mol/s") "Flow rate that enters the  

1067         distillation column";  

1068     Real Fc[Nt,Nc](each unit="mol/s") "Component flow rate that enters the  

1069         column";  

1070     Real B(unit="mol/s") "Bottom Flow Rate";  

1071     Real V[Nt+1](each unit="mol/s") "Vapour flow rate at each stage";  

1072     Real L[Nt](each unit="mol/s") "Liquid flow rate at each stage";  

1073     Real x[Nt,Nc](each unit="-",each start = 1/Nc) "Liquid Composition at  

1074         each stage";  

1075     Real y[Nt+1,Nc](each unit="-",each start = 1/Nc) "Vapour Composition  

1076         at each stage";  

1077     Real Pvap_c[Nt,Nc](each unit="Pa") "Saturation Pressure";  

1078     Real T[Nt](each unit = "K", each min = 0, each start = Tguess)"
```

```

    Temperature at each stage";
1071 Real K_c[Nt,Nc](each unit = "-", each min = 1, each start = 1.5);
1072 Real P[Nt](each unit="Pa")"Pressure at each stage";
1073 Real HSideOut[Nout](each unit="J/mol")"Enthalpy of the Side Streams";
1074 Real HFeed[Nt](each unit="J/mol")"Enthalpy of the Feed";
1075 Real HSide[Nt](each unit="J/mol")"Enthalpy of the Side Stream";
1076 Real FSide[Nt](each unit="mol/s")"Side Stream Flow Rates";
1077 Real correctL[Nt](each unit="mol/s")"Correct Liquid Flow Rates";
1078 Real correctV[Nt](each unit="mol/s")"Correct Vapour Flow Rates";
1079 Real Hvap[Nt,Nc](each unit="J/mol")"Enthalpy of Components present in
      Vapour of each stage";
1080 Real Hliq[Nt,Nc](each unit="J/mol")"Enthalpy of Components present in
      Liquid of each stage";
1081 Real F[Nt](each unit="mol/s")"Feed that enters the Distillation
      Column at each stage";
1082 //=====
1083
1084 Real xdel[Nc-1];
1085 Real a11,a12,a13,a14,a15,a16,a17,a18,a19,a10;
1086 Real xvapin[Ni];
1087 Real pervap[Nt];
1088 Integer b11;
1089 Integer b12,b13,b14,b15,b16,b17;
1090 Real a[Nc+1];
1091 //Thermodynamic Variables:
1092 constant Real R = 1.98721;
1093 Real tau[Nt,Nc, Nc], G[Nt,Nc, Nc], alpha[Nc, Nc], A[Nc, Nc], BIPS[Nc,
      Nc, 2];
1094 Real sum1[Nt,Nc](each start = 1), sum2[Nt,Nc](each start = 1);
1095 Real gma_c[Nt,Nc](each start = 1);
1096
1097 equation
1098 BIPS = Simulator.Files.ThermodynamicFunctions.BIPNRTL(Nc, C.CAS);
1099 A = BIPS[:, :, 1];
1100 alpha = BIPS[:, :, 2];
1101 //===== Pressure at Each Stage
1102
1103 // Pressure at each stage is calculated by interpolation.
1104 P[1]=CondP;
1105 P[Nt]=ReboilerP;
1106 for i in 2:Nt-1 loop
1107   if CondP == ReboilerP then
1108     P[i]=CondP;
1109   else
1110     if ReboilerP > CondP then
1111       P[i]=CondP + ((i - 1)/(Nt -1))*(ReboilerP -CondP);
1112     else
1113       P[i]=CondP + ((i - 1)/(Nt -1))*(CondP -ReboilerP);
1114     end if;
1115   end if;
1116 end for;
1117 //
1118 //=====Determining the Location of the Feed and the Side
1119 Stream=====
1120 if l==Ni then
1121   a11=InT_s[1]+1;
1122   a12=0;
1123   a13=0;

```

```

1124     a14=0;
1125     a15=0;
1126     a16=0;
1127     a17=0;
1128     a18=0;
1129     a19=0;
1130     a10=0;
1131 elseif 2==Ni then
1132     a11=InT_s[1]+1;
1133     a12=InT_s[2]+1;
1134     a13=0;
1135     a14=0;
1136     a15=0;
1137     a16=0;
1138     a17=0;
1139     a18=0;
1140     a19=0;
1141     a10=0;
1142 elseif 3==Ni then
1143     a11=InT_s[1]+1;
1144     a12=InT_s[2]+1;
1145     a13=InT_s[3]+1;
1146     a14=0;
1147     a15=0;
1148     a16=0;
1149     a17=0;
1150     a18=0;
1151     a19=0;
1152     a10=0;
1153 elseif 4==Ni then
1154     a11=InT_s[1]+1;
1155     a12=InT_s[2]+1;
1156     a13=InT_s[3]+1;
1157     a14=InT_s[4]+1;
1158     a15=0;
1159     a16=0;
1160     a17=0;
1161     a18=0;
1162     a19=0;
1163     a10=0;
1164 elseif 5==Ni then
1165     a11=InT_s[1]+1;
1166     a12=InT_s[2]+1;
1167     a13=InT_s[3]+1;
1168     a14=InT_s[4]+1;
1169     a15=InT_s[5]+1;
1170     a16=0;
1171     a17=0;
1172     a18=0;
1173     a19=0;
1174     a10=0;
1175 elseif 6==Ni then
1176     a11=InT_s[1]+1;
1177     a12=InT_s[2]+1;
1178     a13=InT_s[3]+1;
1179     a14=InT_s[4]+1;
1180     a15=InT_s[5]+1;
1181     a16=InT_s[6]+1;
1182     a17=0;
1183     a18=0;
1184     a19=0;
1185     a10=0;
1186 elseif 7==Ni then
1187     a11=InT_s[1]+1;

```

```

1188     a12=InT_s[2]+1;
1189     a13=InT_s[3]+1;
1190     a14=InT_s[4]+1;
1191     a15=InT_s[5]+1;
1192     a16=InT_s[6]+1;
1193     a17=InT_s[7]+1;
1194     a18=0;
1195     a19=0;
1196     a10=0;
1197 elseif 8==Ni then
1198     a11=InT_s[1]+1;
1199     a12=InT_s[2]+1;
1200     a13=InT_s[3]+1;
1201     a14=InT_s[4]+1;
1202     a15=InT_s[5]+1;
1203     a16=InT_s[6]+1;
1204     a17=InT_s[7]+1;
1205     a18=InT_s[8]+1;
1206     a19=0;
1207     a10=0;
1208 elseif 9==Ni then
1209     a11=InT_s[1]+1;
1210     a12=InT_s[2]+1;
1211     a13=InT_s[3]+1;
1212     a14=InT_s[4]+1;
1213     a15=InT_s[5]+1;
1214     a16=InT_s[6]+1;
1215     a17=InT_s[7]+1;
1216     a18=InT_s[8]+1;
1217     a19=InT_s[9]+1;
1218     a10=0;
1219 else
1220     a11=InT_s[1]+1;
1221     a12=InT_s[2]+1;
1222     a13=InT_s[3]+1;
1223     a14=InT_s[4]+1;
1224     a15=InT_s[5]+1;
1225     a16=InT_s[6]+1;
1226     a17=InT_s[7]+1;
1227     a18=InT_s[8]+1;
1228     a19=InT_s[9]+1;
1229     a10=InT_s[10]+1;
1230 end if;
1231 if 1==Nout then
1232     b11=OutT_s[1]+1;
1233     b12=0;
1234     b13=0;
1235     b14=0;
1236     b15=0;
1237     b16=0;
1238     b17=0;
1239 elseif 2==Nout then
1240     b11=OutT_s[1]+1;
1241     b12=OutT_s[2]+1;
1242     b13=0;
1243     b14=0;
1244     b15=0;
1245     b16=0;
1246     b17=0;
1247 elseif 3==Nout then
1248     b11=OutT_s[1]+1;
1249     b12=OutT_s[2]+1;
1250     b13=OutT_s[3]+1;
1251     b14=0;

```

```

1252     b15=0;
1253     b16=0;
1254     b17=0;
1255 elseif 4==Nout then
1256     b11=OutT_s[1]+1;
1257     b12=OutT_s[2]+1;
1258     b13=OutT_s[3]+1;
1259     b14=OutT_s[4]+1;
1260     b15=0;
1261     b16=0;
1262     b17=0;
1263 elseif 5==Nout then
1264     b11=OutT_s[1]+1;
1265     b12=OutT_s[2]+1;
1266     b13=OutT_s[3]+1;
1267     b14=OutT_s[4]+1;
1268     b15=OutT_s[5]+1;
1269     b16=0;
1270     b17=0;
1271 elseif 6==Nout then
1272     b11=OutT_s[1]+1;
1273     b12=OutT_s[2]+1;
1274     b13=OutT_s[3]+1;
1275     b14=OutT_s[4]+1;
1276     b16=OutT_s[6]+1;
1277     b15=0;
1278     b17=0;
1279 elseif 7==Nout then
1280     b11=OutT_s[1]+1;
1281     b12=OutT_s[2]+1;
1282     b13=OutT_s[3]+1;
1283     b14=OutT_s[4]+1;
1284     b15=OutT_s[5]+1;
1285     b16=OutT_s[6]+1;
1286     b17=OutT_s[7]+1;
1287 else
1288     b11=0;
1289     b12=0;
1290     b13=0;
1291     b14=0;
1292     b15=0;
1293     b16=0;
1294     b17=0;
1295 end if;
1296 //
```

```

1297 //=====Determining the Feed Flow Rate at each stage
1298 // If the Feed is entering that particular stage it will be assigned the
1299 // inlet flow rate else it will be assigned the value zero. If a side
// stream is leaving from a particular tray provided that the phase is
// liquid it will be assigned the value provided by the user.
1300 for i in 1:Nt loop
1301   if i==a11 then
1302     Feed[i]=Fin[1];
1303   elseif i==a12 then
1304     Feed[i]=Fin[2];
1305   elseif i==a13 then
1306     Feed[i]=Fin[3];
1307   elseif i==a14 then
1308     Feed[i]=Fin[4];
1309   elseif i==a15 then
```

```

1310     Feed[ i]=Fin [ 5];
1311     elseif i==a16 then
1312     Feed[ i]=Fin [ 6];
1313     elseif i==a17 then
1314     Feed[ i]=Fin [ 7];
1315     elseif i==a18 then
1316     Feed[ i]=Fin [ 8];
1317     elseif i==a19 then
1318     Feed[ i]=Fin [ 9];
1319     elseif i==a10 then
1320     Feed[ i]=Fin [ 10];
1321     elseif i==b11 and SidePhase1 == 1 then
1322     Feed[ i]=(-1*SideF [ 1]);
1323     elseif i==b12 and SidePhase2 == 1 then
1324     Feed[ i]=(-1*SideF [ 2]);
1325     elseif i==b13 and SidePhase3 == 1 then
1326     Feed[ i]=(-1*SideF [ 3]);
1327     elseif i==b14 and SidePhase4 == 1 then
1328     Feed[ i]=(-1*SideF [ 4]);
1329     elseif i==b15 and SidePhase5 == 1 then
1330     Feed[ i]=(-1*SideF [ 5]);
1331     elseif i==b16 and SidePhase6 == 1 then
1332     Feed[ i]=(-1*SideF [ 6]);
1333     elseif i==b17 and SidePhase7 == 1 then
1334     Feed[ i]=(-1*SideF [ 7]);
1335     else
1336     Feed[ i]=0;
1337     end if;
1338   end for;
1339 //===== Determining the Percentage Vapour of the Feed entering the
1340 // paticular stream=====
1340   for i in 1:Nt loop
1341     if i==a11 then
1342       pervap[ i]=xvapin [ 1];
1343     elseif i==a12 then
1344       pervap[ i]=xvapin [ 2];
1345     elseif i==a13 then
1346       pervap[ i]=xvapin [ 3];
1347     elseif i==a14 then
1348       pervap[ i]=xvapin [ 4];
1349     elseif i==a15 then
1350       pervap[ i]=xvapin [ 5];
1351     elseif i==a16 then
1352       pervap[ i]=xvapin [ 6];
1353     elseif i==a17 then
1354       pervap[ i]=xvapin [ 7];
1355     elseif i==a18 then
1356       pervap[ i]=xvapin [ 8];
1357     elseif i==a19 then
1358       pervap[ i]=xvapin [ 9];
1359     elseif i==a10 then
1360       pervap[ i]=xvapin [ 10];
1361     else
1362       pervap[ i]=0;
1363     end if;
1364   end for;
1365   for i in 1:Nc loop
1366     Fc[ 1, i]=0;
1367   end for;
1368 //=====
1369 //=====Overall Material Balance

```

```

1370   if Nout > 0 then
1371     sum(Fin [:])=B+D+sum(SideF [:]);
1372   else
1373     sum(Fin [:])=B+D;
1374   end if;
1375   // =====
1376
1377   // connector equations
1378   for i in 1:Ni loop
1379     In[i].P = Pin[i];
1380     In[i].T = Tin[i];
1381     In[i].H = Hin[i];
1382     In[i].F = Fin[i];
1383     In[i].x_pc[1, :] = x_c[i, :];
1384     In[i].xvap=xvapin[i];
1385   end for;
1386   Dist.P = CondP;
1387   Dist.T = T[1];
1388   Dist.F = D;
1389   Dist.H = Hout1;
1390   Dist.x_pc[1, :] = (integer(x[1, :] .*10000)) ./10000;
1391   Bot.P = P[Nt];
1392   Bot.T = T[Nt];
1393   Bot.F = B;
1394   Bot.H = Hout2;
1395   Bot.x_pc[1, :] = (integer(x[Nt, :] .*10000)) ./10000;
1396   Cduty.Q=Qc;
1397   Rduty.Q=Qr;
1398   // =====
1399
1400   //===== At Condenser
1401
1402   V[1]=L[1]+D;
1403   RR=L[1]/D;
1404   for g in 1:Nc loop
1405     for k in 1:Nc loop
1406       tau[1,g,k] = A[g,k]/(R * T[1]);
1407     end for;
1408   end for;
1409   for i in 1:Nc loop
1410     for j in 1:Nc loop
1411       G[1, i, j] = exp(-alpha[i, j] * tau[1, i, j]);
1412     end for;
1413   end for;
1414   for i in 1:Nc loop
1415     sum1[1, i] = sum(x[1, :] .* G[1, :, i]);
1416     sum2[1, i] = sum(x[1, :] .* tau[1, :, i] .* G[1, :, i]);
1417   end for;
1418   for i in 1:Nc loop
1419     log(gma_c[1, i]) = sum(x[1, :] .* tau[1, :, i] .* G[1, :, i]) / sum(x[1, :]
1420     .* G[1, :, i]) + sum(x[1, :] .* G[1, i, :]) ./ sum1[1, :] .* (tau[1, i,
1421     :] - sum2[1, :] ./ sum1[1, :]));
1422   end for;
1423   for i in 1:Nc loop
1424     Pvap_c[1, i] = Simulator.Files.ThermodynamicFunctions.Psat(C[i].VP,
1425     T[1]);
1426   end for;
1427   for j in 1:Nc loop
1428     K_c[1, j] = gma_c[1, j]*Pvap_c[1, j] / P[1];
1429   end for;
1430   a[1]=0;
1431   for d in 1:Nc loop

```

```

1426     a[d+1]=a[1]+ (x[1,d]*K_c[1,d]);  

1427     end for;  

1428     sum(a[:])=1;  

1429 // _____  

1430 //=====Assumption For Vapor Flow : Equimolar Flow  

1431 for k in 2:Nt+1 loop  

1432     if Nout > 0 and SidePhase1 == 2 and k== b11 then  

1433         V[k]=V[k-1]-SideF[1];  

1434     elseif Nout > 0 and SidePhase2 == 2 and k== b12 then  

1435         V[k]=V[k-1]-SideF[2];  

1436     elseif Nout > 0 and SidePhase3 == 2 and k== b13 then  

1437         V[k]=V[k-1]-SideF[3];  

1438     elseif Nout > 0 and SidePhase4 == 2 and k== b14 then  

1439         V[k]=V[k-1]-SideF[4];  

1440     elseif Nout > 0 and SidePhase5 == 2 and k== b15 then  

1441         V[k]=V[k-1]-SideF[5];  

1442     elseif Nout > 0 and SidePhase6 == 2 and k== b16 then  

1443         V[k]=V[k-1]-SideF[6];  

1444     elseif Nout > 0 and SidePhase7 == 2 and k== b17 then  

1445         V[k]=V[k-1]-SideF[7];  

1446     else  

1447         V[k]=V[k-1]+(Feed[k-1]*pervap[k-1]);  

1448     end if;  

1449     end for;  

1450 // _____  

1451 //=====Calculation of Vapour Composition at Condenser and 1st  

1452 Stage=  

1453 y[1,:]=x[1,:].*K_c[1,:];  

1454 sum(y[2,:])=1;  

1455 for i in 1:Nc-1 loop  

1456 y[2,i]=x[1,i];  

1457 end for;  

1458 // _____  

1459 //=====Calculation from 2nd Stage to Reboiler  

1460 for m in 2:Nt loop  

1461 // Liquid Flow Rate at the paticular stage calculated from material  

1462 // balance at that stage  

1463 if m==Nt then  

1464 L[m]=B;  

1465 else  

1466 L[m]=(Feed[m]*(1-pervap[m]))+L[m-1];  

1467 end if;  

1468 // _____  

1469 //Thermodynamic Calculation at that Stage  

1470 for n in 1:Nc loop  

1471     Pvap_c[m,n] = Simulator.Files.ThermodynamicFunctions.Psat(C[n].VP,  

1472                 T[m]);  

1473     end for;  

1474 // _____  

1475 for g in 1:Nc loop  

1476     for k in 1:Nc loop  

1477         tau[m,g,k] = A[g,k]/ (R * T[m]);  

1478     end for;  

1479 end for;
```

```

1477   for i in 1:Nc loop
1478     for j in 1:Nc loop
1479       G[ m,i, j ] = exp( -alpha[ i, j ] * tau[ m,i, j ] );
1480     end for;
1481   end for;
1482   for i in 1:Nc loop
1483     sum1[ m,i ] = sum( x[ m,:) .* G[ m,:, i ] );
1484     sum2[ m,i ] = sum( x[ m,:] .* tau[ m,:, i ] .* G[ m,:, i ] );
1485   end for;
1486   for i in 1:Nc loop
1487     log( gma_c[ m,i ] ) = sum( x[ m,:] .* tau[ m,:, i ] .* G[ m,:, i ] ) / sum( x[ m,:]
1488       .* G[ m,:, i ] ) + sum( x[ m,:] .* G[ m,i, :] ./ sum1[ m,:] .* ( tau[ m,i,
1489       :] ./ sum2[ m,:] ./ sum1[ m,:] ) );
1490   end for;
1491   //
1492   for p in 1:Nc loop
1493     K_c[ m,p ] = gma_c[ m,p ] * Pvap_c[ m,p ] / P[ m ];
1494   end for;
1495   for q in 1:Nc loop
1496     y[ m,q ] - ( x[ m,q ] * K_c[ m,q ] ) = 0;
1497   end for;
1498   sum( y[ m,:] ./ K_c[ m,:] ) = 1;
1499   //////////////////////////////////////////////////////////////////// Assigning the Inlet Component Flow Rates and Leaving Side Streams
1500   //////////////////////////////////////////////////////////////////// Component Flow Rates
1501   if m==a11 then
1502     for k in 1:Nc loop
1503       Fc[ m,k ] = Fin[ 1 ] * x_c[ 1, k ];
1504     end for;
1505   elseif m==a12 then
1506     for k in 1:Nc loop
1507       Fc[ m,k ] = Fin[ 2 ] * x_c[ 2, k ];
1508     end for;
1509   elseif m==a13 then
1510     for k in 1:Nc loop
1511       Fc[ m,k ] = Fin[ 3 ] * x_c[ 3, k ];
1512     end for;
1513   elseif m==a14 then
1514     for k in 1:Nc loop
1515       Fc[ m,k ] = Fin[ 4 ] * x_c[ 4, k ];
1516     end for;
1517   elseif m==a15 then
1518     for k in 1:Nc loop
1519       Fc[ m,k ] = Fin[ 5 ] * x_c[ 5, k ];
1520     end for;
1521   elseif m==a16 then
1522     for k in 1:Nc loop
1523       Fc[ m,k ] = Fin[ 6 ] * x_c[ 6, k ];
1524     end for;
1525   elseif m==a17 then
1526     for k in 1:Nc loop
1527       Fc[ m,k ] = Fin[ 7 ] * x_c[ 7, k ];
1528     end for;
1529   elseif m==a18 then
1530     for k in 1:Nc loop
1531       Fc[ m,k ] = Fin[ 8 ] * x_c[ 8, k ];
1532     end for;
1533   elseif m==a19 then
1534     for k in 1:Nc loop
1535       Fc[ m,k ] = Fin[ 9 ] * x_c[ 9, k ];
1536     end for;
1537   elseif m==a10 then
1538     for k in 1:Nc loop
1539       Fc[ m,k ] = Fin[ 10 ] * x_c[ 10, k ];
1540     end for;

```

```

1538 elseif m==b11 then
1539   if SidePhase1==2 then
1540     for k in 1:Nc loop
1541       Fc[m,k]=(-1*SideF[1]*y[m,k]);
1542     end for;
1543   else
1544     for k in 1:Nc loop
1545       Fc[m,k]=(-1*SideF[1]*x[m,k]);
1546     end for;
1547   end if;
1548 elseif m==b12 then
1549   if SidePhase2==2 then
1550     for k in 1:Nc loop
1551       Fc[m,k]=(-1*SideF[2]*y[m,k]);
1552     end for;
1553   else
1554     for k in 1:Nc loop
1555       Fc[m,k]=(-1*SideF[2]*x[m,k]);
1556     end for;
1557   end if;
1558 elseif m==b13 then
1559   if SidePhase3==2 then
1560     for k in 1:Nc loop
1561       Fc[m,k]=(-1*SideF[3]*y[m,k]);
1562     end for;
1563   else
1564     for k in 1:Nc loop
1565       Fc[m,k]=(-1*SideF[3]*x[m,k]);
1566     end for;
1567   end if;
1568 elseif m==b14 then
1569   if SidePhase4==2 then
1570     for k in 1:Nc loop
1571       Fc[m,k]=(-1*SideF[4]*y[m,k]);
1572     end for;
1573   else
1574     for k in 1:Nc loop
1575       Fc[m,k]=(-1*SideF[4]*x[m,k]);
1576     end for;
1577   end if;
1578 elseif m==b15 then
1579   if SidePhase5==2 then
1580     for k in 1:Nc loop
1581       Fc[m,k]=(-1*SideF[5]*y[m,k]);
1582     end for;
1583   else
1584     for k in 1:Nc loop
1585       Fc[m,k]=(-1*SideF[5]*x[m,k]);
1586     end for;
1587   end if;
1588 elseif m==b16 then
1589   if SidePhase6==2 then
1590     for k in 1:Nc loop
1591       Fc[m,k]=(-1*SideF[6]*y[m,k]);
1592     end for;
1593   else
1594     for k in 1:Nc loop
1595       Fc[m,k]=(-1*SideF[6]*x[m,k]);
1596     end for;
1597   end if;
1598 elseif m==b17 then
1599   if SidePhase7==2 then
1600     for k in 1:Nc loop
1601       Fc[m,k]=(-1*SideF[7]*y[m,k]);

```

```

1602 end for;
1603 else
1604 for k in 1:Nc loop
1605 Fc[m,k]=(-1*SideF[7]*x[m,k]);
1606 end for;
1607 end if;
1608 else
1609 for l in 1:Nc loop
1610 Fc[m,l]=0;
1611 end for;
1612 end if;
1613 //=====
1614 for r in 1:Nc-1 loop
1615 if (((V[m]*y[m,r])+(L[m]*x[m,r])-Fc[m,r]-(L[m-1]*x[m-1,r]))/V[m+1]) <
1616 0 or (((V[m]*y[m,r])+(L[m]*x[m,r])-Fc[m,r]-(L[m-1]*x[m-1,r]))/V[
1617 m+1]) > 1 then
1618 y[m+1,r]=y[m,r];
1619 else
1620 (L[m-1]*x[m-1,r]) + (V[m+1]*y[m+1,r])+ Fc[m,r]-(V[m]*y[m,r]) - (L[m]*x
1621 [m,r])=0;
1622 end if;
1623 end for;
1624 sum(y[m+1,:])=1;
1625 end for;
1626 //=====
1627 // Conditions:
1628 // Assigning the Condition that the difference between the reboiler
1629 // composition from the calculated value and the obtained value should
1630 // be zero.
1631 for h in 1:Nc-1 loop
1632 xdel[h]=((sum(Fc[:,h]))-(D*x[1,h]))/B;
1633 end for;
1634 for w in 1:Nc-1 loop
1635 x[Nt,w]-xdel[w]=0;
1636 end for;
1637 sum(x[1,:])=1;
1638 //=====Energy Balance Calculation
1639 for i in 1:Nc loop
1640 Hvapcond_c[i] = Simulator.Files.ThermodynamicFunctions.HVapId(C[i].  

1641 SH, C[i].VapCp, C[i].HOV, C[i].Tc, T[2]);
1642 Hliqcond_c[i] = Simulator.Files.ThermodynamicFunctions.HLiqId(C[i].  

1643 SH, C[i].VapCp, C[i].HOV, C[i].Tc, T[1]);
1644 end for;
1645 if Ctype == "Total" then
1646 Hliqcond = Hout1;
1647 elseif Ctype == "Partial" then
1648 Hliqcond = sum(y[2,:]* Hliqcond_c[:]);
1649 end if;
1650 Hvapcond = sum(y[2,:]* Hvapcond_c[:]);
1651 if Nout > 0 then
1652 sum(Fin[:,]* Hin[:]) + Qr - Qc = B * Hout2 + D * Hliqcond + sum(SideF
1653 [:]* HSideOut[:]);
1654 else
1655 sum(Fin[:,]* Hin[:]) - Qr = B * Hout2 + D * Hliqcond + Qc;
1656 end if;
1657 V[1] * Hvapcond = Qc + D * Hliqcond + L[1] * Hout1;
1658 //==Assigning the Obtained Values to the Side Streams if Selected
1659 if Nout == 1 then
1660 Out_s[1].P = P[b11];

```

```

1654 Out_s[1].T = T[b11];
1655 Out_s[1].F = (-1*Feed[b11]);
1656 Out_s[1].H= HSideOut[1];
1657 if SidePhase1==1 then
1658   Out_s[1].x_pc[1, :] = (integer(x[b11,:]*10000)) ./10000;
1659 else
1660   Out_s[1].x_pc[1, :] = (integer(y[b11,:]*10000)) ./10000;
1661 end if;
1662 end if;
1663 if Nout==2 then
1664   Out_s[1].P = P[b11];
1665   Out_s[1].T = T[b11];
1666   Out_s[1].F = (-1*Feed[b11]);
1667   Out_s[1].H= HSideOut[1];
1668 if SidePhase1==1 then
1669   Out_s[1].x_pc[1, :] = (integer(x[b11,:]*10000)) ./10000;
1670 else
1671   Out_s[1].x_pc[1, :] = (integer(y[b11,:]*10000)) ./10000;
1672 end if;
1673 Out_s[2].P = P[b12];
1674 Out_s[2].T = T[b12];
1675 Out_s[2].F = (-1*Feed[b12]);
1676 Out_s[2].H= HSideOut[2];
1677 if SidePhase2==1 then
1678   Out_s[2].x_pc[1, :] = (integer(x[b12,:]*10000)) ./10000;
1679 else
1680   Out_s[2].x_pc[1, :] = (integer(y[b12,:]*10000)) ./10000;
1681 end if;
1682 end if;
1683 if Nout==3 then
1684   Out_s[1].P = P[b11];
1685   Out_s[1].T = T[b11];
1686   Out_s[1].F = (-1*Feed[b11]);
1687   Out_s[1].H= HSideOut[1];
1688 if SidePhase1==1 then
1689   Out_s[1].x_pc[1, :] = (integer(x[b11,:]*10000)) ./10000;
1690 else
1691   Out_s[1].x_pc[1, :] = (integer(y[b11,:]*10000)) ./10000;
1692 end if;
1693 Out_s[2].P = P[b12];
1694 Out_s[2].T = T[b12];
1695 Out_s[2].F = (-1*Feed[b12]);
1696 Out_s[2].H= HSideOut[2];
1697 if SidePhase2==1 then
1698   Out_s[2].x_pc[1, :] = (integer(x[b12,:]*10000)) ./10000;
1699 else
1700   Out_s[2].x_pc[1, :] = (integer(y[b12,:]*10000)) ./10000;
1701 end if;
1702 Out_s[3].P = P[b13];
1703 Out_s[3].T = T[b13];
1704 Out_s[3].F = (-1*Feed[b13]);
1705 Out_s[3].H= HSideOut[3];
1706 if SidePhase3==1 then
1707   Out_s[3].x_pc[1, :] = (integer(x[b13,:]*10000)) ./10000;
1708 else
1709   Out_s[3].x_pc[1, :] = (integer(y[b13,:]*10000)) ./10000;
1710 end if;
1711 end if;
1712 if Nout==4 then
1713   Out_s[1].P = P[b11];
1714   Out_s[1].T = T[b11];
1715   Out_s[1].F = (-1*Feed[b11]);
1716   Out_s[1].H= HSideOut[1];
1717 if SidePhase1==1 then

```

```

1718     Out_s[1].x_pc[1, :] = (integer(x[b11,:]*10000)) ./10000;
1719   else
1720     Out_s[1].x_pc[1, :] = (integer(y[b11,:]*10000)) ./10000;
1721   end if;
1722   Out_s[2].P = P[b12];
1723   Out_s[2].T = T[b12];
1724   Out_s[2].F = (-1*Feed[b12]);
1725   Out_s[2].H= HSideOut[2];
1726   if SidePhase2==1 then
1727     Out_s[2].x_pc[1, :] = (integer(x[b12,:]*10000)) ./10000;
1728   else
1729     Out_s[2].x_pc[1, :] = (integer(y[b12,:]*10000)) ./10000;
1730   end if;
1731   Out_s[3].P = P[b13];
1732   Out_s[3].T = T[b13];
1733   Out_s[3].F = (-1*Feed[b13]);
1734   Out_s[3].H= HSideOut[3];
1735   if SidePhase3==1 then
1736     Out_s[3].x_pc[1, :] = (integer(x[b13,:]*10000)) ./10000;
1737   else
1738     Out_s[3].x_pc[1, :] = (integer(y[b13,:]*10000)) ./10000;
1739   end if;
1740   Out_s[4].P = P[b14];
1741   Out_s[4].T = T[b14];
1742   Out_s[4].F = (-1*Feed[b12]);
1743   Out_s[4].H= HSideOut[4];
1744   if SidePhase4==1 then
1745     Out_s[4].x_pc[1, :] = (integer(x[b14,:]*10000)) ./10000;
1746   else
1747     Out_s[4].x_pc[1, :] = (integer(y[b14,:]*10000)) ./10000;
1748   end if;
1749 end if;
1750 if Nout ==5 then
1751   Out_s[1].P = P[b11];
1752   Out_s[1].T = T[b11];
1753   Out_s[1].F = (-1*Feed[b11]);
1754   Out_s[1].H= HSideOut[1];
1755   if SidePhase1==1 then
1756     Out_s[1].x_pc[1, :] = (integer(x[b11,:]*10000)) ./10000;
1757   else
1758     Out_s[1].x_pc[1, :] = (integer(y[b11,:]*10000)) ./10000;
1759   end if;
1760   Out_s[2].P = P[b12];
1761   Out_s[2].T = T[b12];
1762   Out_s[2].F = (-1*Feed[b12]);
1763   Out_s[2].H= HSideOut[2];
1764   if SidePhase2==1 then
1765     Out_s[2].x_pc[1, :] = (integer(x[b12,:]*10000)) ./10000;
1766   else
1767     Out_s[2].x_pc[1, :] = (integer(y[b12,:]*10000)) ./10000;
1768   end if;
1769   Out_s[3].P = P[b13];
1770   Out_s[3].T = T[b13];
1771   Out_s[3].F = (-1*Feed[b13]);
1772   Out_s[3].H= HSideOut[3];
1773   if SidePhase3==1 then
1774     Out_s[3].x_pc[1, :] = (integer(x[b13,:]*10000)) ./10000;
1775   else
1776     Out_s[3].x_pc[1, :] = (integer(y[b13,:]*10000)) ./10000;
1777   end if;
1778   Out_s[4].P = P[b14];
1779   Out_s[4].T = T[b14];
1780   Out_s[4].F = (-1*Feed[b12]);
1781   Out_s[4].H= HSideOut[4];

```

```

1782 if SidePhase4==1 then
1783   Out_s[4].x_pc[1, :] = (integer(x[b14,:]*10000)) ./10000;
1784 else
1785   Out_s[4].x_pc[1, :] = (integer(y[b14,:]*10000)) ./10000;
1786 end if;
1787 Out_s[5].P = P[b15];
1788 Out_s[5].T = T[b15];
1789 Out_s[5].F = (-1*Feed[b15]);
1790 Out_s[5].H= HSideOut[5];
1791 if SidePhase5==1 then
1792   Out_s[5].x_pc[1, :] = (integer(x[b12,:]*10000)) ./10000;
1793 else
1794   Out_s[5].x_pc[1, :] = (integer(y[b12,:]*10000)) ./10000;
1795 end if;
1796 end if;
1797 if Nout==6 then
1798   Out_s[1].P = P[b11];
1799   Out_s[1].T = T[b11];
1800   Out_s[1].F = (-1*Feed[b11]);
1801   Out_s[1].H= HSideOut[1];
1802 if SidePhase1==1 then
1803   Out_s[1].x_pc[1, :] = (integer(x[b11,:]*10000)) ./10000;
1804 else
1805   Out_s[1].x_pc[1, :] = (integer(y[b11,:]*10000)) ./10000;
1806 end if;
1807 Out_s[2].P = P[b12];
1808 Out_s[2].T = T[b12];
1809 Out_s[2].F = (-1*Feed[b12]);
1810 Out_s[2].H= HSideOut[2];
1811 if SidePhase2==1 then
1812   Out_s[2].x_pc[1, :] = (integer(x[b12,:]*10000)) ./10000;
1813 else
1814   Out_s[2].x_pc[1, :] = (integer(y[b12,:]*10000)) ./10000;
1815 end if;
1816 Out_s[3].P = P[b13];
1817 Out_s[3].T = T[b13];
1818 Out_s[3].F = (-1*Feed[b13]);
1819 Out_s[3].H= HSideOut[3];
1820 if SidePhase3==1 then
1821   Out_s[3].x_pc[1, :] = (integer(x[b13,:]*10000)) ./10000;
1822 else
1823   Out_s[3].x_pc[1, :] = (integer(y[b13,:]*10000)) ./10000;
1824 end if;
1825 Out_s[4].P = P[b14];
1826 Out_s[4].T = T[b14];
1827 Out_s[4].F = (-1*Feed[b12]);
1828 Out_s[4].H= HSideOut[4];
1829 if SidePhase4==1 then
1830   Out_s[4].x_pc[1, :] = (integer(x[b14,:]*10000)) ./10000;
1831 else
1832   Out_s[4].x_pc[1, :] = (integer(y[b14,:]*10000)) ./10000;
1833 end if;
1834 Out_s[5].P = P[b15];
1835 Out_s[5].T = T[b15];
1836 Out_s[5].F = (-1*Feed[b15]);
1837 Out_s[5].H= HSideOut[5];
1838 if SidePhase5==1 then
1839   Out_s[5].x_pc[1, :] = (integer(x[b12,:]*10000)) ./10000;
1840 else
1841   Out_s[5].x_pc[1, :] = (integer(y[b12,:]*10000)) ./10000;
1842 end if;
1843 Out_s[6].P = P[b16];
1844 Out_s[6].T = T[b16];
1845 Out_s[6].F = (-1*Feed[b16]);

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1846 Out_s[6].H= HSideOut[6];
1847 if SidePhase6==1 then
1848     Out_s[6].x_pc[1, :] = (integer(x[b16,:]*10000)) ./10000;
1849 else
1850     Out_s[6].x_pc[1, :] = (integer(y[b16,:]*10000)) ./10000;
1851 end if;
1852 end if;
1853 if Nout==7 then
1854     Out_s[1].P = P[b11];
1855     Out_s[1].T = T[b11];
1856     Out_s[1].F = (-1*Feed[b11]);
1857     Out_s[1].H= HSideOut[1];
1858     if SidePhase1==1 then
1859         Out_s[1].x_pc[1, :] = (integer(x[b11,:]*10000)) ./10000;
1860     else
1861         Out_s[1].x_pc[1, :] = (integer(y[b11,:]*10000)) ./10000;
1862     end if;
1863     Out_s[2].P = P[b12];
1864     Out_s[2].T = T[b12];
1865     Out_s[2].F = (-1*Feed[b12]);
1866     Out_s[2].H= HSideOut[2];
1867     if SidePhase2==1 then
1868         Out_s[2].x_pc[1, :] = (integer(x[b12,:]*10000)) ./10000;
1869     else
1870         Out_s[2].x_pc[1, :] = (integer(y[b12,:]*10000)) ./10000;
1871     end if;
1872     Out_s[3].P = P[b13];
1873     Out_s[3].T = T[b13];
1874     Out_s[3].F = (-1*Feed[b13]);
1875     Out_s[3].H= HSideOut[3];
1876     if SidePhase3==1 then
1877         Out_s[3].x_pc[1, :] = (integer(x[b13,:]*10000)) ./10000;
1878     else
1879         Out_s[3].x_pc[1, :] = (integer(y[b13,:]*10000)) ./10000;
1880     end if;
1881     Out_s[4].P = P[b14];
1882     Out_s[4].T = T[b14];
1883     Out_s[4].F = (-1*Feed[b12]);
1884     Out_s[4].H= HSideOut[4];
1885     if SidePhase4==1 then
1886         Out_s[4].x_pc[1, :] = (integer(x[b14,:]*10000)) ./10000;
1887     else
1888         Out_s[4].x_pc[1, :] = (integer(y[b14,:]*10000)) ./10000;
1889     end if;
1890     Out_s[5].P = P[b15];
1891     Out_s[5].T = T[b15];
1892     Out_s[5].F = (-1*Feed[b15]);
1893     Out_s[5].H= HSideOut[5];
1894     if SidePhase5==1 then
1895         Out_s[5].x_pc[1, :] = (integer(x[b12,:]*10000)) ./10000;
1896     else
1897         Out_s[5].x_pc[1, :] = (integer(y[b12,:]*10000)) ./10000;
1898     end if;
1899     Out_s[6].P = P[b16];
1900     Out_s[6].T = T[b16];
1901     Out_s[6].F = (-1*Feed[b16]);
1902     Out_s[6].H= HSideOut[6];
1903     if SidePhase6==1 then
1904         Out_s[6].x_pc[1, :] = (integer(x[b16,:]*10000)) ./10000;
1905     else
1906         Out_s[6].x_pc[1, :] = (integer(y[b16,:]*10000)) ./10000;
1907     end if;
1908     Out_s[7].P = P[b17];
1909     Out_s[7].T = T[b17];

```

```

1910 Out_s[7].F = (-1*Feed[b12]);  

1911 Out_s[7].H= HSideOut[7];  

1912 if SidePhase7==1 then  

1913     Out_s[7].x_pc[1, :] = (integer(x[b17,:]*10000)) ./10000;  

1914 else  

1915     Out_s[7].x_pc[1, :] = (integer(y[b17,:]*10000)) ./10000;  

1916 end if;  

1917 end if;  

1918 //————— Correct Flow Rates through  

1919 Energy Balance —————  

1920 for i in 1:Nt loop  

1921     if i==a11 then  

1922         HFeed[i]=Hin[1];  

1923         F[i]=Fin[1];  

1924     elseif i==a12 then  

1925         HFeed[i]=Hin[2];  

1926         F[i]=Fin[2];  

1927     elseif i==a13 then  

1928         HFeed[i]=Hin[3];  

1929         F[i]=Fin[3];  

1930     elseif i==a14 then  

1931         HFeed[i]=Hin[4];  

1932         F[i]=Fin[4];  

1933     elseif i==a15 then  

1934         HFeed[i]=Hin[5];  

1935         F[i]=Fin[5];  

1936     elseif i==a16 then  

1937         HFeed[i]=Hin[6];  

1938         F[i]=Fin[6];  

1939     elseif i==a17 then  

1940         HFeed[i]=Hin[7];  

1941         F[i]=Fin[7];  

1942     elseif i==a18 then  

1943         HFeed[i]=Hin[8];  

1944         F[i]=Fin[8];  

1945     elseif i==a19 then  

1946         HFeed[i]=Hin[9];  

1947         F[i]=Fin[9];  

1948     elseif i==a10 then  

1949         HFeed[i]=Hin[10];  

1950         F[i]=Fin[10];  

1951     else  

1952         HFeed[i]=0;  

1953         F[i]=0;  

1954     end if;  

1955 end for;  

1956 for i in 1:Nt loop  

1957     if i==b11 then  

1958         HSide[i]=HSideOut[1];  

1959         FSide[i]=SideF[1];  

1960     elseif i==b12 then  

1961         HSide[i]=HSideOut[2];  

1962         FSide[i]=SideF[2];  

1963     elseif i==b13 then  

1964         HSide[i]=HSideOut[3];  

1965         FSide[i]=SideF[3];  

1966     elseif i==b14 then  

1967         HSide[i]=HSideOut[4];  

1968         FSide[i]=SideF[4];  

1969     elseif i==b15 then  

1970         HSide[i]=HSideOut[5];  

1971         FSide[i]=SideF[5];  

1972     elseif i==b16 then  

1973         HSide[i]=HSideOut[6];

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```

1973   FSide[ i]=SideF[ 6];
1974   elseif i==b17 then
1975     HSide[ i]=HSideOut[ 7];
1976     FSide[ i]=SideF[ 7];
1977   else
1978     HSide[ i]=0;
1979     FSide[ i]=0;
1980   end if;
1981   end for;
1982   for j in 1:Nt loop
1983     for i in 1:Nc loop
1984       Hvap[ j,i ] = Simulator.Files.ThermodynamicFunctions.HVapId( C[ i ].SH, C[
1985         i ].VapCp, C[ i ].HOV, C[ i ].Tc, T[ j ] );
1986       Hliq[ j,i ] = Simulator.Files.ThermodynamicFunctions.HLiqId( C[ i ].SH, C[
1987         i ].VapCp, C[ i ].HOV, C[ i ].Tc, T[ j ] );
1988     end for;
1989   end for;
1990   correctL[ 1]=L[ 1 ];
1991   correctV[ 1]=0;
1992   correctV[ 2]=V[ 1 ];
1993   correctL[ Nt]=B;
1994   //=====Energy Balance at each stage
1995   for i in 2:Nt-1 loop
1996     F[ i ]+correctL[ i-1 ]+correctV[ i+1 ]-correctV[ i ]-correctL[ i ]-FSide[ i ]=0;
1997     (F[ i ]*HFeed[ i ]) +(correctL[ i-1 ]*sum( Hliq[ i-1, : ].*x[ i-1, : ] )) +(correctV[ i
1998       +1]*sum( Hvap[ i+1, : ].*y[ i+1, : ] )) -(correctV[ i ]*sum( Hvap[ i, : ].*y[ i,
1999       : ] )) -(correctL[ i ]*sum( Hliq[ i, : ].*x[ i, : ] )) -(FSide[ i ]*HSide[ i ]) =0;
1996   end for;
1997   //
1998   end NRTL;
1999 end DistCol;

```

```

1 package PengPxy
2 model Pxy
3 //Model Description:
4
5 //Pxy is a binary phase diagram where the Temperature is held constant and
6 //the Liquid Phase Mole Fraction is varied. For a particular liquid phase
7 //mole fraction the Pressure and Vapour phase mole fraction is obtained
8 //through thermodynamic realationship at equilibrium conditions.
9 //
10 //====User Input Data=====
11 extends Modelica.Icons.Example;
12 import data = Simulator.Files.ChemsepDatabase;
13 parameter data.Propane eth;
14 parameter data.Nbutane prop;
15 parameter Integer Nc = 2"Number of Components";
16 parameter Real Temp(unit="K")=323"Temperature";
17 parameter Integer NOP=6;//Number of Points
18 parameter data.GeneralProperties C[Nc] = {eth, prop};
19 parameter Real step=0.2;//Step Value
20 //====Model Variables=====
21 points point[NOP](each Nc = Nc, each C = C,each T = Temp);
22 Real x[NOP,Nc](each unit="--")"Liquid Phase Mole Fraction";
23 Real y[NOP,Nc](each unit="--")"Vapour Phase Mole Fraction";
24 Real P[NOP](each unit="Pa")"Pressure";
25 //====Equation Section=====
26 equation
27 for i in 1:NOP loop
28     x[i, 1] = 0 + (i - 1) * step;
29     x[i, 2]=1-x[i, 1];
30 end for;
31 for i in 1:NOP loop
32     point[i].x=x[i, :];
33     point[i].P=P[i];
34     point[i].y=y[i, :];
35 end for;
36
37 end Pxy;
38 model points
39     parameter Integer Nc"Number of Components";
40     parameter Simulator.Files.ChemsepDatabase.GeneralProperties C[Nc];
41     parameter Real T(unit="K")"Temperature";
42     Real P(unit="Pa",min= Simulator.Files.ThermodynamicFunctions.Psat(C[1].
43         VP, T),max=Simulator.Files.ThermodynamicFunctions.Psat(C[2].VP, T),
44         start=Simulator.Files.ThermodynamicFunctions.Psat(C[1].VP, T))"Pressure";
45     Real x[2](each unit="--")"Liquid Phase Mole Fraction";
46     Real y[2](each min=0,each max=1,each start=0.5)"Vapour Phase Mole
47     Fraction";
48     parameter Real kij_c[Nc, Nc](each start = 1) =
49         Simulator.Files.ThermodynamicFunctions.BIPPR(Nc, C.name);
50     Real Tr_c[Nc](each start = Tg) "Reduced temperature";
51     Real b_c[Nc];
52     Real a_c[Nc](each start = xg);
53     Real m_c[Nc];
54     Real q_c[Nc];
55     Real aij_c[Nc, Nc];
56     Real K_c[Nc](each start = K_guess);
57     Real aMliq, bMliq;
58     Real Aliq(each start=xliq), Bliq(each start=xvapg);

```

```

55  Real Cliq[4];
56  Real Z_RL[3, 2](start=xliqg);
57  Real Zliq[3](each start=xliqg), Zll(each start=xvapg);
58  Real sumxliq[Nc];
59  Real aMvap, bMvap;
60  Real Avap(each start=xliqg), Bvap(each start=xvapg);
61  Real Cvap[4];
62  Real Z_RV[3, 2](each start= xvapg);
63  Real Zvap[3](each start=xvapg), Zvv;
64  Real sumxvap[Nc];
65  Real A, B, Cdummy, D_c[Nc], E, F, G, H_c[Nc], I_c[Nc], J_c[Nc];
66  Real R=8.314;
67  Real philiq_c[Nc];
68  Real phivap_c[Nc];
69  extends Simulator.GuessModels.InitialGuess;
70 equation
71   Tr_c = T ./ C.Tc;
72   b_c = 0.0778 * R * C.Tc ./ C.Pc;
73   m_c = 0.37464 .+ 1.54226 * C.AF .- 0.26992 * C.AF .^ 2;
74   q_c = 0.45724 * R ^ 2 * C.Tc .^ 2 ./ C.Pc;
75   a_c = q_c .* (1 + m_c .* (1 - sqrt(Tr_c))) .^ 2;
76   aij_c = {{(1 - kij_c[i, j]) * sqrt(a_c[i] * a_c[j])} for i in 1:Nc} for
77   j in 1:Nc;
78 //=====
79 //Liquid_Fugacity Coefficient Calculation Routine
80 aMliq = sum({{x[i] * x[j] * aij_c[i, j]} for i in 1:Nc} for j in 1:Nc);
81 bMliq = sum(b_c .* x[:]);
82 Aliq = aMliq * P / (R * T) ^ 2;
83 Bliq = bMliq * P / (R * T);
84 Cliq[1] = 1;
85 Cliq[2] = Bliq - 1;
86 Cliq[3] = Aliq - 3 * Bliq ^ 2 - 2 * Bliq;
87 Cliq[4] = Bliq ^ 3 + Bliq ^ 2 - Aliq * Bliq;
88 Z_RL = Modelica.Math.Vectors.Utilities.roots(Cliq);
89 Zliq = {Z_RL[i, 1]} for i in 1:3;
90 Zll = min({Zliq});
91 sumxliq = {sum({x[j] * aij_c[i, j]} for j in 1:Nc)} for i in 1:Nc;
92 A = Zll + 2.4142135 * Bliq;
93 B = Zll - 0.414213 * Bliq;
94 Cdummy = log(Zll - Bliq);
95 for i in 1:Nc loop
96   D_c[i] = b_c[i] / bMliq;
97 end for;
98 for i in 1:Nc loop
99   J_c[i] = sumxliq[i] / aMliq;
end for;
100 philiq_c = exp(Aliq / (Bliq * sqrt(8)) * log(A / B) .* (D_c .- 2 * J_c)
101   .+ (Zll - 1) * D_c .- Cdummy);
102 //=====
103 //Vapour Fugacity Calculation Routine
104 aMvap = sum({{y[i] * y[j] * aij_c[i, j]} for i in 1:Nc} for j in 1:Nc);
105 bMvap = sum(b_c .* y[:]);
106 Avap = aMvap * P / (R * T) ^ 2;
107 Bvap = bMvap * P / (R * T);
108 Cvap[1] = 1;
109 Cvap[2] = Bvap - 1;
110 Cvap[3] = Avap - 3 * Bvap ^ 2 - 2 * Bvap;
111 Cvap[4] = Bvap ^ 3 + Bvap ^ 2 - Avap * Bvap;
112 Z_RV = Modelica.Math.Vectors.Utilities.roots(Cvap);
113 Zvap = {Z_RV[i, 1]} for i in 1:3;
114 Zvv = max({Zvap});
115 sumxvap = {sum({y[j] * aij_c[i, j]} for j in 1:Nc)} for i in 1:Nc;
116   E = Zvv + 2.4142135 * Bvap;

```

```

117      F = Zvv - 0.414213 * Bvap;
118      G = log(Zvv - Bvap);
119      for i in 1:Nc loop
120          H_c[i] = b_c[i] / bMvap;
121      end for;
122      for i in 1:Nc loop
123          I_c[i] = sumxvap[i] / aMvap;
124      end for;
125      phivap_c = exp(Avap / (Bvap * sqrt(8)) * log(E / F) .* (H_c .- 2 * I_c)
126          .+ (Zvv - 1) * H_c .- G);
127      for i in 1:Nc loop
128          K_c[i] = philiq_c[i] / phivap_c[i];
129      end for;
130      y[:] = x[:] .* K_c[:];
131      sum(y[:]) = 1;
132  end points;
133 end PengPxy;

```

```

1 package PengTxy
2 model Txy
3 //Model Description:
4
5 //Txy is a binary phase diagram where the Pressure is held constant and the
6 //Liquid Phase Mole Fraction is varied. For a particular liquid phase
7 //mole fraction the Temperature and Vapour phase mole fraction is
8 //obtained through thermodynamic realationship at equillbrium conditions.
9 //
10 //=====User Input Data=====
11 extends Modelica.Icons.Example;
12 import data = Simulator.Files.ChemsepDatabase;
13 parameter data.Ethane eth;
14 parameter data.Propane prop;
15 parameter Integer Nc = 2"Number of Components";
16 parameter Real Pressure(unit="Pa")=101325"Pressure";
17 parameter Integer NOP=6"Number of Points";
18 parameter data.GeneralProperties C[Nc] = {eth, prop};
19 parameter Real step=0.2;
20
21 //=====Model Variables=====
22 points point[NOP](each Nc = Nc, each C = C,each P = Pressure,each Tb1=
23 Tb1,each Tb2=Tb2);
24 Real x[NOP,Nc];
25 Real y[NOP,Nc];
26 Real T[NOP];
27 extends PengTxy.intialguess;// The intial guess values are the boiling
28 // point temperature of pure components.The pressure in the intialguess
29 // should be changed as per requirement.
30 //=====Equation Section=====
31 equation
32 for i in 1:NOP loop
33     x[i, 1] = 0 + (i - 1) * step;
34     x[i, 2]=1-x[i, 1];
35 end for;
36 for i in 1:NOP loop
37     point[i].x=x[i, :];
38     point[i].T=T[i];
39     point[i].y=y[i, :];
40 end for;
41
42 end Txy;
43 model points
44 parameter Integer Nc;
45 parameter Simulator.Files.ChemsepDatabase.GeneralProperties C[Nc];
46 parameter Real P;
47 parameter Real Tb1;
48 parameter Real Tb2;
49 Real T(min=Tb1,max=Tb2,start=Tb1);
50 Real x[2];
51 Real y[2](each min=0,each max=1,each start=0.4);
52 parameter Real kij_c[Nc, Nc](each start = 1) =
53     Simulator.Files.ThermodynamicFunctions.BIPPR(Nc, C.name);
54     Real Tr_c[Nc](each start = Tg) "Reduced temperature";
55     Real b_c[Nc];
56     Real a_c[Nc](start = xg);
57     Real m_c[Nc];
58     Real q_c[Nc];
59     Real aij_c[Nc, Nc];

```

```

56  Real K_c[Nc]( start = 1);
57  Real aMliq, bMliq;
58  Real Aliq, Bliq;
59  Real Cliq[4];
60  Real Z_RL[3, 2]( start=xliq );
61  Real Zliq[3], Zll;
62  Real sumxliq[Nc];
63  Real aMvap, bMvap;
64  Real Avap, Bvap;
65  Real Cvap[4];
66  Real Z_RV[3, 2];
67  Real Zvap[3], Zvv;
68  Real sumxvap[Nc];
69  Real A, B, Cdummy, D_c[Nc], E, F, G, H_c[Nc], I_c[Nc], J_c[Nc];
70  Real R=8.314;
71  Real philiq_c[Nc](each start=5);
72  Real phivap_c[Nc](each start=5);
73  extends Simulator.GuessModels.InitialGuess;
74 equation
75   Tr_c = T ./ C.Tc;
76   b_c = 0.0778 * R * C.Tc ./ C.Pc;
77   m_c = 0.37464 .+ 1.54226 * C.AF .- 0.26992 * C.AF .^ 2;
78   q_c = 0.45724 * R ^ 2 * C.Tc .^ 2 ./ C.Pc;
79   a_c = q_c .* (1 + m_c .* (1 - sqrt(Tr_c))) .^ 2;
80   aij_c = {{(1 - kij_c[i, j]) * sqrt(a_c[i] * a_c[j])} for i in 1:Nc} for
81   j in 1:Nc};
82 //=====
83 //Liquid_Fugacity Coefficient Calculation Routine
84 aMliq = sum({{x[i] * x[j] * aij_c[i, j]} for i in 1:Nc} for j in 1:Nc);
85 bMliq = sum(b_c .* x[:]);
86 Aliq = aMliq * P / (R * T) ^ 2;
87 Bliq = bMliq * P / (R * T);
88 Cliq[1] = 1;
89 Cliq[2] = Bliq - 1;
90 Cliq[3] = Aliq - 3 * Bliq ^ 2 - 2 * Bliq;
91 Cliq[4] = Bliq ^ 3 + Bliq ^ 2 - Aliq * Bliq;
92 Z_RL = Modelica.Math.Vectors.Utilities.roots(Cliq);
93 Zliq = {Z_RL[i, 1]} for i in 1:3;
94 Zll = min({Zliq});
95 sumxliq = {sum({x[j] * aij_c[i, j]} for j in 1:Nc)} for i in 1:Nc;
96 A = Zll + 2.4142135 * Bliq;
97 B = Zll - 0.414213 * Bliq;
98 Cdummy = log(Zll - Bliq);
99 for i in 1:Nc loop
100   D_c[i] = b_c[i] / bMliq;
101 end for;
102 for i in 1:Nc loop
103   J_c[i] = sumxliq[i] / aMliq;
104 end for;
105   philiq_c = exp(Aliq / (Bliq * sqrt(8)) * log(A / B) .* (D_c .- 2 * J_c)
106   .+ (Zll - 1) * D_c .- Cdummy);
107 //=====
108 //Vapour Fugacity Calculation Routine
109 aMvap = sum({{y[i] * y[j] * aij_c[i, j]} for i in 1:Nc} for j in 1:Nc);
110 bMvap = sum(b_c .* y[:]);
111 Avap = aMvap * P / (R * T) ^ 2;
112 Bvap = bMvap * P / (R * T);
113 Cvap[1] = 1;
114 Cvap[2] = Bvap - 1;
115 Cvap[3] = Avap - 3 * Bvap ^ 2 - 2 * Bvap;
116 Cvap[4] = Bvap ^ 3 + Bvap ^ 2 - Avap * Bvap;
117 Z_RV = Modelica.Math.Vectors.Utilities.roots(Cvap);

```

```

118 Zvv = max({Zvap});
119 sumxvap = {sum({y[j] * aij_c[i, j] for j in 1:Nc}) for i in 1:Nc};
120 E = Zvv + 2.4142135 * Bvap;
121 F = Zvv - 0.414213 * Bvap;
122 G = log(Zvv - Bvap);
123 for i in 1:Nc loop
124   H_c[i] = b_c[i] / bMvap;
125 end for;
126 for i in 1:Nc loop
127   I_c[i] = sumxvap[i] / aMvap;
128 end for;
129 phivap_c = exp(Avap / (Bvap * sqrt(8)) * log(E / F) .* (H_c .- 2 * I_c)
130   .+ (Zvv - 1) * H_c .- G);
131 for i in 1:Nc loop
132   K_c[i] = philiq_c[i] / phivap_c[i];
133 end for;
134 y[:] = x[:] .* K_c[:];
135 sum(y[:]) = 1;
136 end points;
137 model intialguess
138 protected
139 //=====User Input Data=====
140 parameter Real P(unit="Pa")=101325;
141 //=====Intial Guess Variables=====
142 parameter Real Tb1(fixed=false);
143 parameter Real Tb2(fixed=false);
144 initial equation
145 log(P)=(C[1].VP[2] + C[1].VP[3] / Tb1 + C[1].VP[4] * log(Tb1) + C[1].VP[5]
146   * Tb1^ C[1].VP[6]);
147 log(P)=(C[2].VP[2] + C[2].VP[3] / Tb2 + C[2].VP[4] * log(Tb2) + C[2].VP[5]
148   * Tb2^ C[2].VP[6]);
149 end intialguess;
150 end PengTxy;

```

```

1 package EqReactor
2 model EquilibriumReactor "Model of an equilibrium reactor to calculate the
3   outlet stream mole fraction of components"
4   extends Simulator.Files.Icons.EquilibriumReactor;
5   //EquilibriumReactor Code works for all the valid phases and all modes
6   //available in DWSIM
7   //The reaction basis included are PartialPressure, Activity and
8   //MoleFraction
9   //The base component need not be specified and is directly calculated
10  //from an external function
11  //
12  //

13  parameter Simulator.Files.ChemsepDatabase.GeneralProperties C[Nc] "
14    Component instances array" annotation(
15      Dialog(tab = "Reactor Specifications", group = "Component Parameters"
16        ));
17  parameter Integer Nc "Number of components" annotation(
18      Dialog(tab = "Reactor Specifications", group = "Component Parameters"
19        ));
20  //
21  //

22  extends Simulator.GuessModels.InitialGuess;
23  //Connector Variables
24  Real Pin(unit = "Pa", min = 0, start = Pg) "Inlet stream pressure";
25  Real Tin(unit = "K", min = 0, start = Tg) "Inlet stream temperature";
26  Real Fin(unit = "mol/s", min = 0, start = Fg) "Inlet stream molar flow
27  rate";
28  Real Hin(unit = "kJ/kmol", start = Htotg) "Inlet stream molar enthalpy"
29  ;
30  Real Sin(unit = "kJ/[kmol.K]") "Inlet stream molar entropy";
31  Real xin_c[Nc](each unit = "K", each min = 0, each max = 1, start = xg)
32  "Inlet stream component mole fraction";
33  Real xvapin;
34  Real Pout(unit = "Pa", min = 0, start = Pg) "Outlet stream pressure";
35  Real Tout(unit = "K", min = 0, start = Tg) "Outlet stream temperature";
36  Real Fout(unit = "mol/s", min = 0, start = Fg) "Outlet stream molar
37  flow rate";
38  Real Hout(unit = "kJ/kmol", start = Htotg) "Outlet stream molar
39  enthalpy";
40  Real Sout(unit = "kJ/[kmol.K]") "Outlet stream molar entropy";
41  Real xout_c[Nc](each unit = "=", each min = 0, each max = 1, start = xg)
42  "Outlet stream component mole fraction";
43  Real xvapout;
44  Real Q;
45  //Model Variables
46  Real Psat[Nc] "Vapour Pressure";
47  Real Kmod[Nr] "Modified Equilibrium Contant";
48  Real Fin_c[Nc] "Component Molar Flow Rates";
49  Real Hr "Reaction Heat";
50  //Model Parameters
51  parameter String Phase = "Vapour" "Required phase:
52    ''Liquid'', ''Vapour''" annotation(
53      Dialog(tab = "Reactions", group = "Equilibrium Reaction Parameters"))
54    ;
55  parameter String Basis = "Activity" "Required basis: ''MoleFraction'',
56    ''Activity'', ''PartialPressure''" annotation(
57      Dialog(tab = "Reactions", group = "Equilibrium Reaction Parameters"))
58    ;
59  parameter String Mode = "Isothermal" "Required mode of operation: ''
60    Isothermal'', ''OutletTemperature'', ''Adiabatic''" annotation(
61      Dialog(tab = "Reactor Specifications", group = "Calculation
62      Parameters")));

```

```

43  parameter Real Pdel(unit = "Pa") = 0 "Pressure drop" annotation(
44    Dialog(tab = "Reactor Specifications", group = "Calculation
45      Parameters"));
46  parameter Real Tdef(unit = "K") = 300 "Defined outlet temperature,
47    applicable if OutletTemperature mode is chosen" annotation(
48    Dialog(tab = "Reactor Specifications", group = "Calculation
49      Parameters"));
50 // Reaction Variables
51 Real SC_rc[Nr, Nc] "Stoichiometric coefficients of the components";
52 Integer BC_r[Nr] "Base component of reaction";
53 Real Ndel[Nr];
54 Real Scabs[Nr, Nc] "Relative stoichiometry with respect to base
55   component";
56 Real Ext_r[Nr](each start = xvapg) "Reaction Extent";
57 Real X_r[Nr, Nc] "Conversion of reactants";
58 // _____
59
60 extends EqReactor.EquilibriumReaction(Nr = 1, Coef_cr = {{-1}, {-1},
61   {1}, {1}}, Rmode = "ConstantK", Kg = {0.5}, T = Tout, P = Pout);
62 Simulator.Files.Interfaces.matConn Out(Nc = Nc) annotation(
63   Placement(visible = true, transformation(origin = {100, 0}, extent =
64     {{-10, -10}, {10, 10}}, rotation = 0), iconTransformation(origin
65     = {100, 0}, extent = {{-10, -10}, {10, 10}}, rotation = 0)));
66 Simulator.Files.Interfaces.enConn enConn annotation(
67   Placement(visible = true, transformation(origin = {2, -100}, extent =
68     {{-10, -10}, {10, 10}}, rotation = 0), iconTransformation(origin
69     = {0, -130}, extent = {{-10, -10}, {10, 10}}, rotation = 0)));
70 Simulator.Files.Interfaces.matConn In(Nc = Nc) annotation(
71   Placement(visible = true, transformation(origin = {-98, -2}, extent =
72     {{-10, -10}, {10, 10}}, rotation = 0), iconTransformation(origin
73     = {-100, -2}, extent = {{-10, -10}, {10, 10}}, rotation = 0)));
74 // _____
75
76 equation
77 // _____
78
79 In.P = Pin;
80 In.T = Tin;
81 In.F = Fin;
82 In.H = Hin;
83 In.S = Sin;
84 In.x_pc[1, :] = xin_c;
85 In.xvap = xvapin;
86 Out.P = Pout;
87 Out.T = Tout;
88 Out.F = Fout;
89 Out.H = Hout;
90 Out.S = Sout;
91 Out.x_pc[1, :] = xout_c;
92 Out.xvap = xvapout;
93 enConn.Q = Q;
94 Pout = Pin - Pdel;
95 for i in 1:Nc loop
96   Psat[i] = Simulator.Files.ThermodynamicFunctions.Psat(C[i].VP, Tin);
97 end for;
98 //Automated calculation of base component
99 for i in 1:Nc loop
100   Fin_c[i] = Fin * xin_c[i];
101 end for;
102 for i in 1:Nr loop
103   BC_r[i] = Simulator.Files.Models.ReactionManager.BaseCalc(Nc, Fin_c,
104

```

```

        SC_rc[ i, :]) ;
90    end for;
91    for j in 1:Nr loop
92      for i in 1:Nc loop
93        SC_rc[j, i] = Coef_cr[i, j];
94      end for;
95    end for;
96  //
```

```

97  for i in 1:Nr loop
98    Ndel[i] = sum(SC_rc[ i, 1:Nc]);
99  end for;
100 if Mode == "Isothermal" then
101   Tout = Tin;
102   Hr = Hr_r[1] * 1E-3 * (Fin_c[BC_r[1]] * X_r[1, BC_r[1]]) / Coef_cr[
103     BC_r[1], 1] * Coef_cr[BC_r[1], 1];
104   Q = Hout * Fout * 1E-3 - Hin * Fin * 1E-3 - Hr;
105 else
106   if Mode == "OutletTemperature" then
107     Tout = Tdef;
108     Hr = Hr_r[1] * 1E-3 * (Fin_c[BC_r[1]] * X_r[1, BC_r[1]]) / Coef_cr[
109       BC_r[1], 1] * Coef_cr[BC_r[1], 1];
110   Q = Hout * Fout * 1E-3 - Hin * Fin * 1E-3 - Hr;
111 else
112   Q = 0;
113   Hr = Hr_r[1] * 1E-3 * (Fin_c[BC_r[1]] * X_r[1, BC_r[1]]) / Coef_cr[
114     BC_r[1], 1] * Coef_cr[BC_r[1], 1];
115   Q = Hout * Fout * 1E-3 - Hin * Fin * 1E-3 - Hr;
116 end if;
117 for i in 1:Nr loop
118   for j in 1:Nc loop
119     Scabs[i, j] = SC_rc[ i, j] / abs(SC_rc[ i, BC_r[ i]]);
120   end for;
121 end for;
122 if Phase == "Vapour" then
123   if Basis == "MoleFraction" then
124     for i in 1:Nr loop
125       Kmod[i] = K[i];
126       Kmod[i] = product((xin_c + Ext_r * Scabs) .^ SC_rc[ i, 1:Nc]) / (1
127         + sum(Ext_r * Scabs)) ^ sum(SC_rc[ i, 1:Nc]);
128     end for;
129   else
130     if Basis == "Activity" then
131       for i in 1:Nr loop
132         Kmmod[i] = K[i] / (Pin / 101325) ^ Ndel[i];
133         Kmmod[i] = product((xin_c + Ext_r * Scabs) .^ SC_rc[ i, 1:Nc]) /
134           (1 + sum(Ext_r * Scabs)) ^ sum(SC_rc[ i, 1:Nc]);
135       end for;
136     else
137       for i in 1:Nr loop
138         Kmmod[i] = K[i] / Pout ^ Ndel[i];
139         Kmmod[i] = product((xin_c + Ext_r * Scabs) .^ SC_rc[ i, 1:Nc]) /
140           (1 + sum(Ext_r * Scabs)) ^ sum(SC_rc[ i, 1:Nc]);
141       end for;
142     end if;
143   end if;
144 else
145   if Basis == "MoleFraction" then
146     for i in 1:Nr loop
147       Kmmod[i] = K[i];
148       Kmmod[i] = product((xin_c + Ext_r * Scabs) .^ SC_rc[ i, 1:Nc]) / (1
149         + sum(Ext_r * Scabs)) ^ sum(SC_rc[ i, 1:Nc]);
```

```

144     end for;
145 else
146     if Basis == "Activity" then
147         for i in 1:Nr loop
148             Kmod[i] = K[i] / Pout ^ (-Ndel[i]);
149             Kmod[i] = product((Psat .* (xin_c + Ext_r * Scabs)) .^ SC_rc[i,
150                             1:Nc]) / (1 + sum(Ext_r * Scabs)) ^ sum(SC_rc[i, 1:Nc]);
151         end for;
152     else
153         for i in 1:Nr loop
154             Kmod[i] = K[i];
155             Kmod[i] = product((Psat .* (xin_c + Ext_r * Scabs)) .^ SC_rc[i,
156                             1:Nc]) / (1 + sum(Ext_r * Scabs)) ^ sum(SC_rc[i, 1:Nc]);
157         end for;
158     end if;
159 end if;
160 Fout = (1 + sum(Ext_r * Scabs)) * Fin;
161 for i in 1:Nc loop
162     xout_c[i] = (xin_c[i] + Ext_r * Scabs[1:Nr, i]) * (Fin / Fout);
163 end for;
164 for j in 1:Nr loop
165     for i in 1:Nc loop
166         if SC_rc[j, i] < 0 then
167             X_r[j, i] = (Fin * xin_c[i] - Fout * xout_c[i]) / (Fin * xin_c[i
168                 ]);
169         else
170             X_r[j, i] = 0;
171         end if;
172     end for;
173 end for;
174 //
```

```

173 end EquilibriumReactor;
174 model EquilibriumReaction "Model of an equilibrium reaction used in
175   equilibrium reactor"
176 //
```

```

176 import Simulator.Files.*;
177 import data = Simulator.Files.ChemsepDatabase;
178 parameter Integer Nr "Number of reactions" annotation(
179     Dialog(tab = "Reactions", group = "Equilibrium Reaction Parameters"))
180     ;
181 parameter Real Coef_cr[Nc, Nr] "Stoichiometric coefficient of
182   components" annotation(
183     Dialog(tab = "Reactions", group = "Equilibrium Reaction Parameters"))
184     ;
185 parameter String Rmode = "ConstantK" "Mode of specifying equilibrium
186   constant: 'ConstantK', 'Tempfunc', 'Gibbs'" annotation(
187     Dialog(tab = "Reactions", group = "Equilibrium Reaction Parameters"))
188     ;
188 parameter Real Kg[Nr] "Equilibrium Constant, applicable if ConstantK is
189   chosen in Rmode" annotation(
190     Dialog(tab = "Reactions", group = "Equilibrium Reaction Parameters"))
191     ;
191 parameter Real A[Nr, 4] "Coefficient of A in equation logk =(A1 + A2*T
192     + A3*T^2 + A4*logT)/(B1 + B2*T + B3*T^2 + B4*logT), applicable if
193     Tempfunc is chosen in Rmode" annotation(
194     Dialog(tab = "Reactions", group = "Equilibrium Reaction Parameters"))
195     ;
195 parameter Real B[Nr, 4] "Coefficient of B in equation logk =(A1 + A2*T
196     + A3*T^2 + A4*logT)/(B1 + B2*T + B3*T^2 + B4*logT), applicable if
197     Tempfunc is chosen in Rmode" annotation(
198     Dialog(tab = "Reactions", group = "Equilibrium Reaction Parameters"))
```

```

Tempfunc is chosen in Rmode" annotation(  

189 Dialog(tab = "Reactions", group = "Equilibrium Reaction Parameters"))  

190 ;  

191 Real T;  

192 //Stoichiometry of reactions  

193 Real Schk_r[Nr];  

194 //Returns whether the specified stoichiometry is correct  

195 Real Hf_c[Nc];  

196 Real Hr_r[Nr];  

197 //Equilibrium Constant  

198 Real K[Nr](start = xliqg);  

199 Real N[Nr](each start = Fg), D[Nr](each start = Fg);  

200 extends Simulator.GuessModels.InitialGuess;  

201 //Variables for Calculating K from Gibbs Free Energy  

202 Real a[Nc], b[Nc], c[Nc], d[Nc];  

203 Real DelH25[Nr](each unit = "J/mol") "Standard Enthalpy at 298.15 K";  

204 Real DelS25[Nr](each unit = "J/mol.K") "Standard Entropy at 298.15 K";  

205 Real DelG25[Nr](each unit = "J/mol.K") "Standard Gibbs Free Energy at  

206 298.15 K";  

207 Real Dela[Nr](each unit = "");  

208 Real Delb[Nr](each unit = "");  

209 Real Delc[Nr](each unit = "");  

210 Real Deld[Nr](each unit = "");  

211 Real CpDelt[Nr](each unit = "J/mol") "Value of Integral Cp*dT";  

212 Real P(unit = "Pa") "Pressure at the Outlet";  

213 Real CpTDelT[Nr](each unit = "J/mol.K") "Value of Integral (Cp/T)*dT";  

214 Real DelH[Nr](each unit = "J/mol") "Enthalpy at Reaction Conditions";  

215 Real DelS[Nr](each unit = "J/mol.K") "Entropy at Reaction Conditions";  

216 Real DelG[Nr](each unit = "J/mol") "Gibbs Energy at Reaction Conditions  

217 ";  

218 Real Ka[Nr](each unit = "") "Equillbrium constant";  

219 equation  

220 //Check of stoichiometric balance  

221 Schk_r = Simulator.Files.Models.ReactionManager.Stoichiometrycheck(Nr,  

222 Nc, C[:,].MW, Coef_cr);  

223 // Calculation of Heat of Reaction  

224 Hf_c [:] = C[:,].IGHF .* 1E-3;  

225 //  



---


226 for i in 1:Nr loop  

227     Hr_r[i] = sum(Hf_c [:] .* Coef_cr[:, i]) / Coef_cr[BC_r[1], i];  

228 end for;  

229 if Rmode == "ConstantK" then  

230     K = Kg;  

231     for i in 1:Nr loop  

232         N[i] = 0;  

233         D[i] = 0;  

234     end for;  

235     //Gibbs Energy Values are assigned the value zero  

236     for i in 1:Nc loop  

237         a[i] = 0;  

238         b[i] = 0;  

239         c[i] = 0;  

240         d[i] = 0;  

241     end for;  

242     for i in 1:Nr loop  

243         DelH25[i] = 0;  

244         DelS25[i] = 0;  

245         DelG25[i] = 0;  

246         Dela[i] = 0;  

247         Delb[i] = 0;  

248         Delc[i] = 0;  

249         Deld[i] = 0;

```

```

246 CpDelT[ i ] = 0;
247 CpTDelT[ i ] = 0;
248 DelH[ i ] = 0;
249 DelS[ i ] = 0;
250 DelG[ i ] = 0;
251 Ka[ i ] = 0;
252 end for;
253 elseif Rmode == "Gibbs" then
254   if Phase == "Vapour" then
255     ( a, b, c, d ) = EqReactor.VapCpdata( Nc, C[ : ].SN );
256   else
257     ( a, b, c, d ) = EqReactor.LiqCpdata( Nc, C[ : ].SN );
258   end if;
259   for i in 1:Nr loop
260     DelH25[ i ] = sum( Coef_cr[ :, i ] .* C[ : ].IGHF / 1000 );
261     DelS25[ i ] = sum( Coef_cr[ :, i ] .* C[ : ].AS / 1000 );
262     DelG25[ i ] = sum( Coef_cr[ :, i ] .* C[ : ].GEF / 1000 );
263   end for;
264   for i in 1:Nr loop
265     Dela[ i ] = sum( Coef_cr[ :, i ] .* a[ : ] );
266     Delb[ i ] = sum( Coef_cr[ :, i ] .* b[ : ] );
267     Delc[ i ] = sum( Coef_cr[ :, i ] .* c[ : ] );
268     Deld[ i ] = sum( Coef_cr[ :, i ] .* d[ : ] );
269   end for;
270   for i in 1:Nr loop
271     //Cp=aT^3+bT^2+cT+d
272     CpDelT[ i ] = Dela[ i ] * ( T ^ 4 - 298.15 ^ 4 ) * 0.25 + Delb[ i ] * ( T ^ 3 - 298.15 ^ 3 ) * ( 1 / 3 ) + Delc[ i ] * ( T ^ 2 - 298.15 ^ 2 ) * 0.5 + Deld[ i ] * ( T - 298.15 );
273     CpTDelT[ i ] = Deld[ i ] * log( T / 298.15 ) + Delc[ i ] * ( T - 298.15 ) + Delb[ i ] * ( T ^ 2 - 298.15 ^ 2 ) * 0.5 + Dela[ i ] * ( T ^ 3 - 298.15 ^ 3 ) * ( 1 / 3 );
274   end for;
275   for i in 1:Nr loop
276     DelH[ i ] = DelH25[ i ] + CpDelT[ i ];
277     DelS[ i ] = DelS25[ i ] + CpTDelT[ i ];
278     DelG[ i ] = DelH[ i ] - T * DelS[ i ];
279   end for;
280   for i in 1:Nr loop
281     Ka[ i ] = exp( -DelG[ i ] / ( 8.314 * T ) );
282   end for;
283   for i in 1:Nr loop
284     N[ i ] = 0;
285     D[ i ] = 0;
286     K[ i ] = Ka[ i ] / ( P / 10 ^ 5 ) ^ sum( Coef_cr[ :, i ] );
287   end for;
288   elseif Rmode == "Tempfunc" then
289     for i in 1:Nr loop
290       N[ i ] = A[ i, 1 ] + A[ i, 2 ] * T + A[ i, 3 ] * T ^ 2 + A[ i, 4 ] * log( T );
291       D[ i ] = B[ i, 1 ] + B[ i, 2 ] * T + B[ i, 3 ] * T ^ 2 + B[ i, 4 ] * log( T );
292     end for;
293     K = exp( N ./ D );
294     for i in 1:Nc loop
295       a[ i ] = 0;
296       b[ i ] = 0;
297       c[ i ] = 0;
298       d[ i ] = 0;
299     end for;
300     for i in 1:Nr loop
301       DelH25[ i ] = 0;
302       DelS25[ i ] = 0;
303       DelG25[ i ] = 0;
304       Dela[ i ] = 0;
305       Delb[ i ] = 0;

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306     Delc[ i ] = 0;
307     Deld[ i ] = 0;
308     CpDelT[ i ] = 0;
309     CpTDelT[ i ] = 0;
310     DelH[ i ] = 0;
311     DelS[ i ] = 0;
312     DelG[ i ] = 0;
313     Ka[ i ] = 0;
314   end for;
315 end if;
316 annotation(
317   Icon(coordinateSystem(initialScale = 0)),
318   Documentation(info = "<html><head></head><body>The <b>
Equilibrium Reaction</b>&nbsp;defined is used in the equilibrium
reactor for the following purposes:</div><div><ul><li>Check if
the stoichiometry specified for the reaction is balanced</li><li>
Calculate the heat of formation</li><li>Calculate the heat of
reaction</li></ul></div><div><br></div>In an equilibrium reaction
model, following calculation parameters are defined:<div><ol><li>
Number of Reactions (<b>Nr</b>)</li><li>Stoichiometric
Coefficient of Components in Reaction (<b>Coef_cr</b>)</li><li>
Mode of specifying Equilibrium Constant (<b>Rmode</b>)</li><li>
Equilibrium Constant (<b>Kg</b>) (<!--StartFragment--><span style =
\"font-size: 12px;\">If Equilibrium Constant mode is ConstantK</
span>)</li><li>Temperature function coefficients (<b>A</b> and <b>
B</b>)&nbsp;(<span style=\"font-size: 12px;\">If Equilibrium
Constant mode is Tempfunc</span>)</li></ol><div><div style=\"
font-size: 12px; orphans: 2; widows: 2;\"><span style=\"orphans:
auto; widows: auto;\">All the above variables are of type <i>
parameter Real </i>except Mode of specifying Equilibrium Constant
(<b>Rmode</b>) which&nbsp;</span><span style=\"orphans: auto;
widows: auto;\"> is of type&nbsp;</span><i style=\"orphans: auto;
widows: auto;\"> parameter String </i><span style=\"orphans: auto;
widows: auto;\">. It can have either of the sting values among
following:</span></div><!--StartFragment--><div style=\"font-size :
12px; orphans: 2; widows: 2;\"><ol><li><b>ConstantK</b>: If the
equilibrium constant is defined directly</li><li><b>Tempfunc</b
>: If the equilibrium constant is to be calculated from given
function of temperature</li></ol></div><!--EndFragment--><div
style=\"font-size: 12px; orphans: 2; widows: 2;\"><br></div><div
style=\"font-size: 12px; orphans: 2; widows: 2;\">During
simulation, their values can specified directly under&nbsp;<b>
Reactions </b><tab>&nbsp;</b>by double clicking on the reactor
model instance.</div></div></div><div style=\"font-size: 12px;
orphans: 2; widows: 2;\"><br></div><div style=\"font-size: 12px;
orphans: 2; widows: 2;\"><br></div><div><br></div></body></html>" );
319 end EquilibriumReaction;
320 end EqReactor;

```